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APPENDIX A

NUMERICAL SIMULATION OF THE WORLD OCEAN CIRCULATION

by

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Abstract

A multi-level model, based on the primitive equations, is developed for simulating the temperature and velocity fields produced in the world ocean by differential heating and surface wind stress. The model ocean has constant depth, free slip at the lower boundary, and neglects momentum advection; so that there is no energy exchange between the barotropic and baroclinic components of the motion, although the former influences the latter through temperature advection.

The ocean model was designed to be coupled to the UCLA atmospheric general circulation model, for the study of the dynamics of climate and climate changes. But here, the model is tested by prescribing the observed seasonally varying surface wind stress and the incident solar radiation, the surface air temperature and humidity, cloudiness and the surface wind speed, which, together with the predicted ocean surface temperature, determine the surface flux of radiant energy, sensible heat and latent heat. From an initial state, in which the temperature as a function of depth and latitude is given, the integration is carried forward over several decades of simulated time, which is longer than the adjustment time scale for the upper levels of the model. In this test, the model successfully simulates most of the large scale features of the world ocean circulation, including a good simulation of the ocean surface temperature.

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Introduction

Governing equations

With momentum advection neglected, and with the Boussinesq approximation for the density and incompressibility, the governing equations are

$$\frac{\partial \psi}{\partial t} = - \frac{1}{\rho_0} \nabla p - 2\Omega \times \psi + f^F , \quad (1)$$

$$\frac{\partial p}{\partial z} = - g \rho , \quad (2)$$

$$\rho = \rho_0 (1 - \alpha |T - T_0|) , \quad (3)$$

$$\frac{\partial T}{\partial t} + \nabla \cdot (T \psi) + \frac{\partial}{\partial z} (Tw) = \frac{Q}{C} , \quad (4)$$

and

$$\nabla \cdot \psi + \frac{\partial w}{\partial z} = 0 , \quad (5)$$

where ψ is horizontal velocity, w is vertical velocity, p is pressure, ρ is density and ρ_0 is a constant, T is temperature and T_0 is a constant, Ω is the earth's rotation vector, g is the acceleration of gravity, α is the coefficient of thermal expansion, and c is the specific heat of sea water. z is the positive upward vertical coordinate and t is time. F is the horizontal frictional force per unit mass and Q is the rate of heating per unit mass, which are taken as

$$F = A_M \nabla^2 \psi + K \frac{\partial^2 \psi}{\partial z^2} , \quad (6)$$

and

$$Q = c A_H \nabla^2 T + \frac{cK}{\delta} \frac{\partial^2 T}{\partial z^2} , \quad (7)$$

where A_M is the coefficient of horizontal eddy viscosity, A_H is the coefficient of horizontal eddy heat diffusion, and K is the coefficient of both the vertical eddy viscosity and the vertical eddy heat diffusion. The coefficient δ (in 7) is defined as

$$\delta \begin{cases} = 1 & \text{when } \frac{\partial T}{\partial z} \geq 0 \\ = 0 & \text{when } \frac{\partial T}{\partial z} < 0 \end{cases}$$

as a parameterization of strong vertical mixing that restores a neutral stratification whenever a vertically unstable stratification develops.

The boundary conditions at the ocean bottom ($z = H$) are

$$w = 0 , \quad (8)$$

$$\frac{\partial \psi}{\partial z} = 0 , \quad (9)$$

and

$$\frac{\partial T}{\partial z} = 0 , \quad (10)$$

so that there is no vertical motion, no momentum transfer and no heat transfer across the lower boundary.

The boundary conditions at the ocean surface ($z = 0$) are

$$w = 0 , \quad (11)$$

$$\frac{\partial \Psi}{\partial z} = \frac{\mathcal{V}_s}{\rho_o K} , \quad (12)$$

and

$$\frac{\partial T}{\partial z} = \frac{Q_s}{c K \rho} , \quad (13)$$

where \mathcal{V}_s is the vector wind stress and Q_s is the downward heat flux at the ocean surface. Setting $w = 0$ at the ocean surface filters out external gravity waves and allows the use of a long computational time step.

The boundary conditions at the lateral walls are zero normal velocity and zero tangential velocity, and zero heat transfer through the walls.

Calculational procedure

The assumption of no momentum advection, constant depth, and free slip at the lower boundary, decouples the barotropic component of the velocity (the vertical mean of the horizontal velocity) from the baroclinic component of the velocity (the deviation of the horizontal velocity from its vertical mean). The former is governed entirely by the wind stress curl and is independent of the heating, while the latter is governed by both the stress and the heating. There is no energy exchange between the two components, although the barotropic

component affects the baroclinic component through the horizontal temperature advection (Eq. 4).

The barotropic component of the velocity is obtained by taking the curl of the vertical integral of Eq. 1, or

$$\frac{\partial M}{\partial t} = - \frac{1}{\rho_0} \nabla P - 2\Omega \times M + \frac{\zeta_s}{\rho_0} + A_M \nabla^2 M , \quad (14)$$

where

$$M = \int_{-H}^0 \psi dz \quad \text{and} \quad P = \int_{-H}^0 p dz ,$$

and

$$\frac{\partial}{\partial t} \nabla^2 \Phi = - f \frac{\partial \Phi}{\partial \lambda} + \frac{1}{\rho_0} \mathbf{k} \cdot \nabla \times \zeta_s + A_M \nabla^4 \Phi , \quad (15)$$

where $\mathbf{k} \times \nabla \Phi = M$ defines the stream function Φ of the vertically integrated velocity M , $f = 2\Omega \sin \varphi$ is the coriolis parameter, λ is longitude and φ is latitude, \mathbf{k} is unit vertical vector, and a is the Earth's radius. This vorticity equation, for the barotropic component of the velocity, is solved as an initial-value boundary-value problem in the way which is described below.

The baroclinic component of the velocity is obtained by substituting for $\psi = \bar{\psi} + \psi'$ and $\nabla p = \bar{\nabla p} + (\nabla p)'$ in Eq. 1, where the bar denotes the vertical mean from $z = -H$ to $z = 0$, and the prime denotes the deviation from the vertical mean. Then, subtracting the vertical mean of Eq. 1, we obtain

$$\frac{\partial \psi'}{\partial t} = - \frac{1}{\rho_0} (\nabla p)' - 2\Omega \times \psi' + A_M \nabla^2 \psi' + \left(K \frac{\partial^2 \psi'}{\partial z^2} - \frac{\zeta_s}{\rho_0 H} \right) , \quad (16)$$

which is the prediction equation for the baroclinic component of the velocity,

The temperature is obtained from Eq. 4.

$(\nabla p)'$ is found by taking the horizontal gradient of Eq. 2, $\partial(\nabla p)/\partial z = -g\nabla\rho$, integrating over the entire depth of the ocean from an arbitrary value of ∇p at $z = -H$, and subtracting the vertical mean, $\overline{\nabla p}$. This insures that the vertical mean of $(\nabla p)'$ is identically zero.

The vertical velocity w is calculated by Eq. 5.

Grid structure, domain, and finite difference scheme

The finite difference calculations are made using spherical coordinates and the same grid structure that was used by Haney (1971a). As shown in Figure 1, the T , p , Φ , and w points are located at the coast lines. The \overline{V} and V' points match the distribution of the horizontal velocity points of the UCLA atmospheric general circulation model, and therefore include points on the equator. In the atmospheric model the horizontal grid size is 4° in latitude and 5° in longitude; but in the ocean model the zonal grid size is reduced to 2.5° in longitude to obtain a somewhat better resolution of the western boundary currents.

The model ocean is divided into five layers, which lie between 0, 70, 380, 960, 2020 and 4000 m in depth, and the horizontal velocities and temperatures are predicted for each layer. To calculate the vertical eddy diffusions of momentum and heat, these velocities and temperatures are attributed to the 20, 120, 640, 1280 and 2760 m depths. The vertical velocities are calculated at the interfaces of the five layers.

The horizontal domain extends from $66^\circ S$ to $74^\circ N$, which excludes the Arctic Ocean. The northern boundary follows the edge of the continental shelf of the composite landmass of North and South America, Europe, Africa and Asia.

The southern boundary approximately follows the edge of the continental shelf of Antarctica. New Zealand, and Australia combined with New Guinea, are retained as islands.

The finite differencing scheme is the same as the one used by Haney (1971a), except that his nine point specification of the vorticity of the barotropic velocity component, which was almost the same as a 45° rotated five point scheme, is here replaced by the usual nearest five point scheme. This prevents a computationally false two grid point noise from being produced by the irregular lateral boundaries and irregular wind stress.

The time integration is carried forward by the leap-frog scheme, with the Euler-backward scheme applied every five time steps.

Prescribed parameters

The prescribed constant parameters are given in Table I.

Table I. Prescribed Constants

$g = 980 \text{ cm/sec}^2$	$T_o = 0^\circ\text{C}$
$\Omega = 7.29 \times 10^{-5} \text{ sec}^{-1}$	$H = 4 \times 10^5 \text{ cm}$
$R = 6.37 \times 10^8 \text{ cm}$	$A_M = 10^9 \text{ cm}^2/\text{sec}$
$c = 0.93 \text{ cal/cm/degr}$	$A_H = 2.5 \times 10^7 \text{ cm}^2/\text{sec}$
$\alpha = 2.5 \times 10^{-4} \text{ degr}^{-1}$	$K = 1 \text{ cm}^2/\text{sec}$
$\rho_o = 1 \text{ gm/cm}^3$	$\Delta t = 40 \text{ min, 8 hours}$

40 minutes is the time step for the integration of the vorticity equation for the barotropic velocity component, and 8 hours is the time step for the integration of the primitive equations for the baroclinic velocity component.

When the oceanic model will be coupled to the atmospheric general circulation model, the surface wind stress will be determined by the atmospheric model. But, here, for the purpose of testing the oceanic model, the surface wind stress is taken as the observed seasonally varying stress given by Hellerman (1967, 1968). Hellerman's values of the mean wind stress for the four seasons of the year (Dec-Jan-Feb; Mar-Apr-May; June-July-Aug; Sept-Oct-Nov) are subjectively interpolated and extrapolated to cover the domain of the oceanic model. A 1-2-1 zonal filter is used to remove some of the two grid interval noise in Hellerman's tabulations. Then, at each grid point, the four seasonal values of Z_s are used to calculate the annual mean and the amplitude and phase of the first annual harmonic of the stress; and from these parameters the surface wind stress is prescribed as a time varying function of the model year.

Q_s , the net downward heat flux at the ocean surface, has four components,

$$Q_s = Q_I - (Q_B + Q_F + Q_L), \quad (17)$$

where Q_I is the net downward flux of solar radiation, Q_B is the net upward flux of infrared radiation, Q_F is the net upward flux of sensible heat, and Q_L is the net upward flux of latent heat.

When the oceanic model will be coupled to the atmospheric general circulation model, the net fluxes of solar and infrared radiation at the ocean surface will depend on the atmospheric state parameters in the fairly complex way given by Katayama (1973). In the present test of the ocean model, however, we use the relatively simple formulations, given by Angstrom (1922) for the solar radiation flux,

$$Q_I = Q_{I_0} \left(1 - 0.7 \frac{C}{8}\right) \left(1 - A_s\right), \quad (18)$$

and by Brunt (1952) for the infrared radiation flux,

$$Q_B = \sigma T_s^4 \times 0.985 [0.39 - 0.05 e^{\frac{1}{2}}] \times [1 - 0.6 (C/8)^2] \quad (19)$$

Where Q_{I_0} is the direct plus indirect solar radiation reaching the ground through a cloudless atmosphere, C is the number of octants of the sky covered by clouds, A_s is the albedo of the ocean surface, σ is the Stefan-Boltzman constant; and e is the vapor pressure of the air (in mb) at 10 m above the ocean surface.

The annual mean and the amplitude and phase of the first annual harmonic of Q_{I_0} are obtained from the Smithsonian Meteorological Tables (1966, tables 133 and 136), with an atmospheric transmission coefficient of 0.7. The albedo of the ocean surface is taken as 0.07.

The annual mean and the amplitude and phase of the first annual harmonic of the number of octants of the sky covered by clouds, C , are calculated from the charts in the cloud atlas of Miller (1971).

The annual mean and the amplitude and phase of the first annual harmonic of the atmospheric vapor pressure, e , are calculated from tabulations of the surface air dewpoint temperature in the atlases of Taljaard et. al. (1969) and Crutcher and Meserve (1970).

These time varying parameters are used, in Eqs. 18 and 19, to prescribe the net flux of solar radiation and to calculate the net flux of infrared radiation at the ocean surface.

For the sensible and latent heat fluxes, the formulations for the test calculations are nearly the same as those that will be used with the combined atmospheric and oceanic models,

$$Q_F = \rho_A C_D C_p |V_A| (T_s - T_A) , \quad (20)$$

and

$$Q_L = \rho_A C_D L |V_A| (q_s^* - q_A) , \quad (21)$$

where ρ_A is the surface air density, $C_D (= 1.23 \times 10^{-3})$ is the surface drag coefficient, C_p is the specific heat of air, $|\psi_A|$ is the surface air speed, L is the latent heat of evaporation, q_s^* is the saturation water vapor mixing ratio at the ocean surface temperature, and q_A is the water vapor mixing ratio of the surface air.

The annual means and the phases and amplitudes of the first annual harmonics of T_A and q_A are calculated from tabulations of the surface air temperature and the surface air dewpoint temperature in the atlases of Taljaard et. al. (1969) and Crutcher and Meserve (1970). The annual mean and the phase and amplitude of the first annual harmonic of the surface (scalar) wind speed are calculated from data in the atlas of MacDonald (1934, charts 27 through 30).

The simulated barotropic circulation

The simulated baroclinic circulation

The simulated surface heat flux

Summary and conclusions

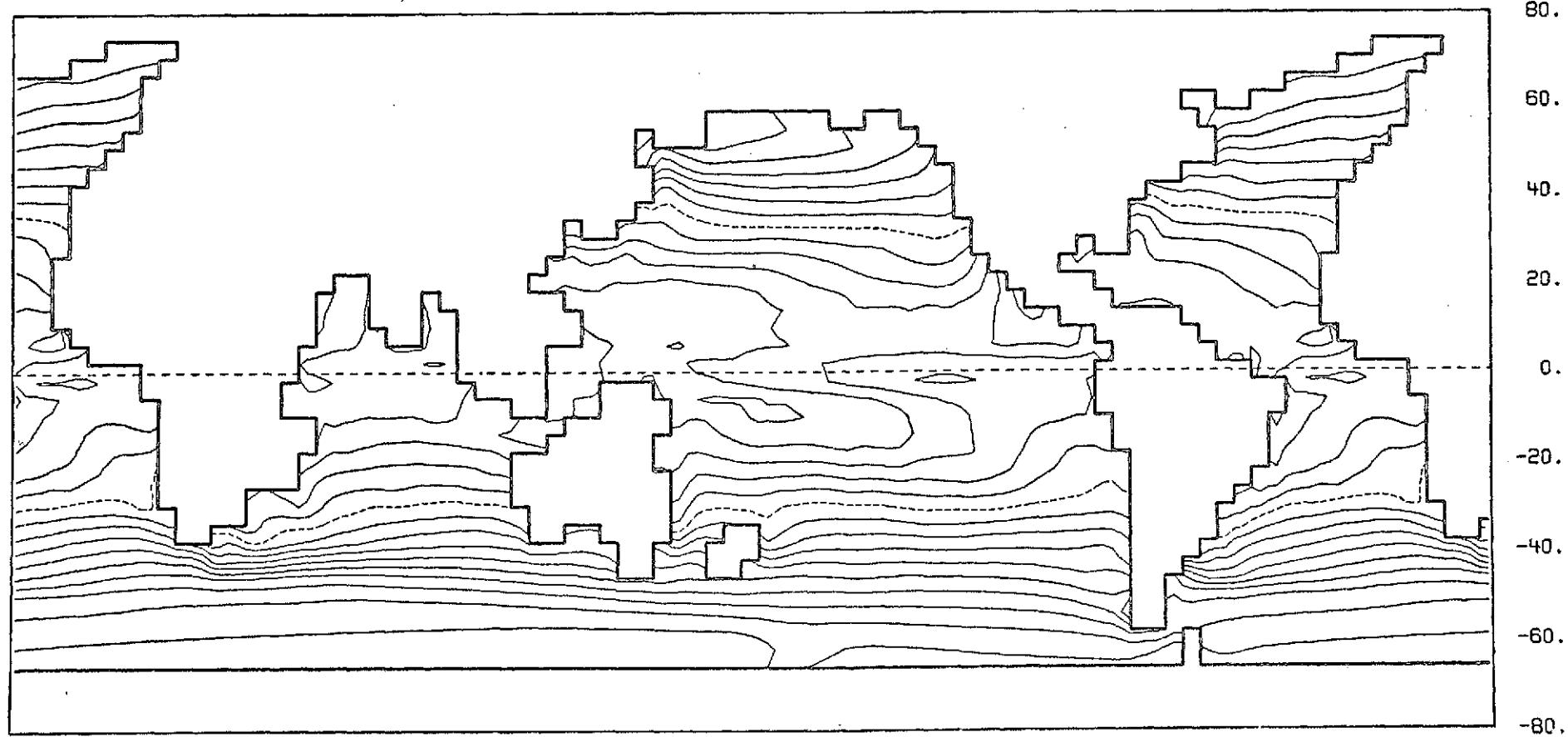
Acknowledgments

References

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DAY = 8773.7

TEMPERATURE AT LEVEL 1 (DEG CENT)
CONTOUR INTERVAL = 2.0 (SOLID LINES)

DASHED LINE = 20.0



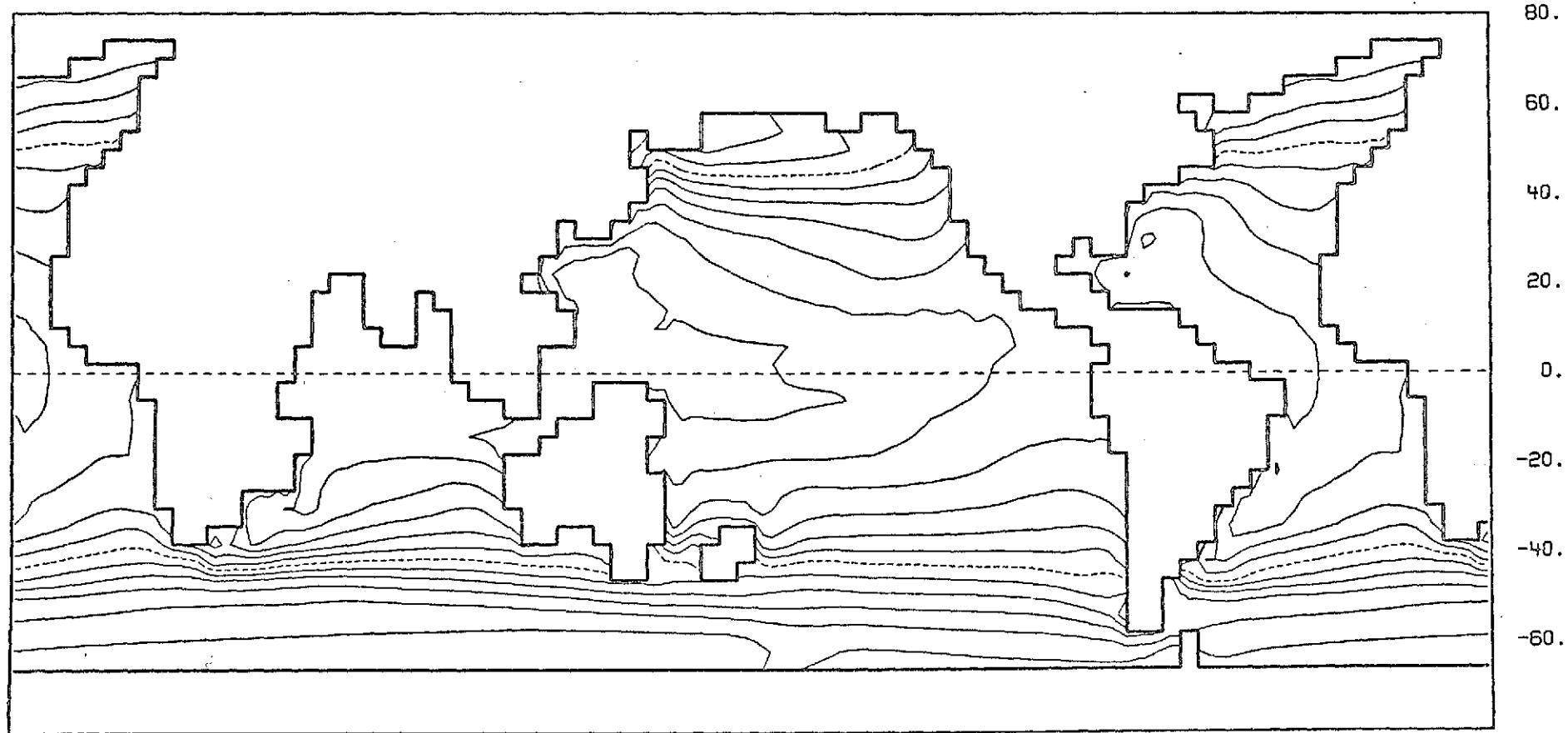
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TEMPERATURE AT LEVEL 2 (DEG CENT)

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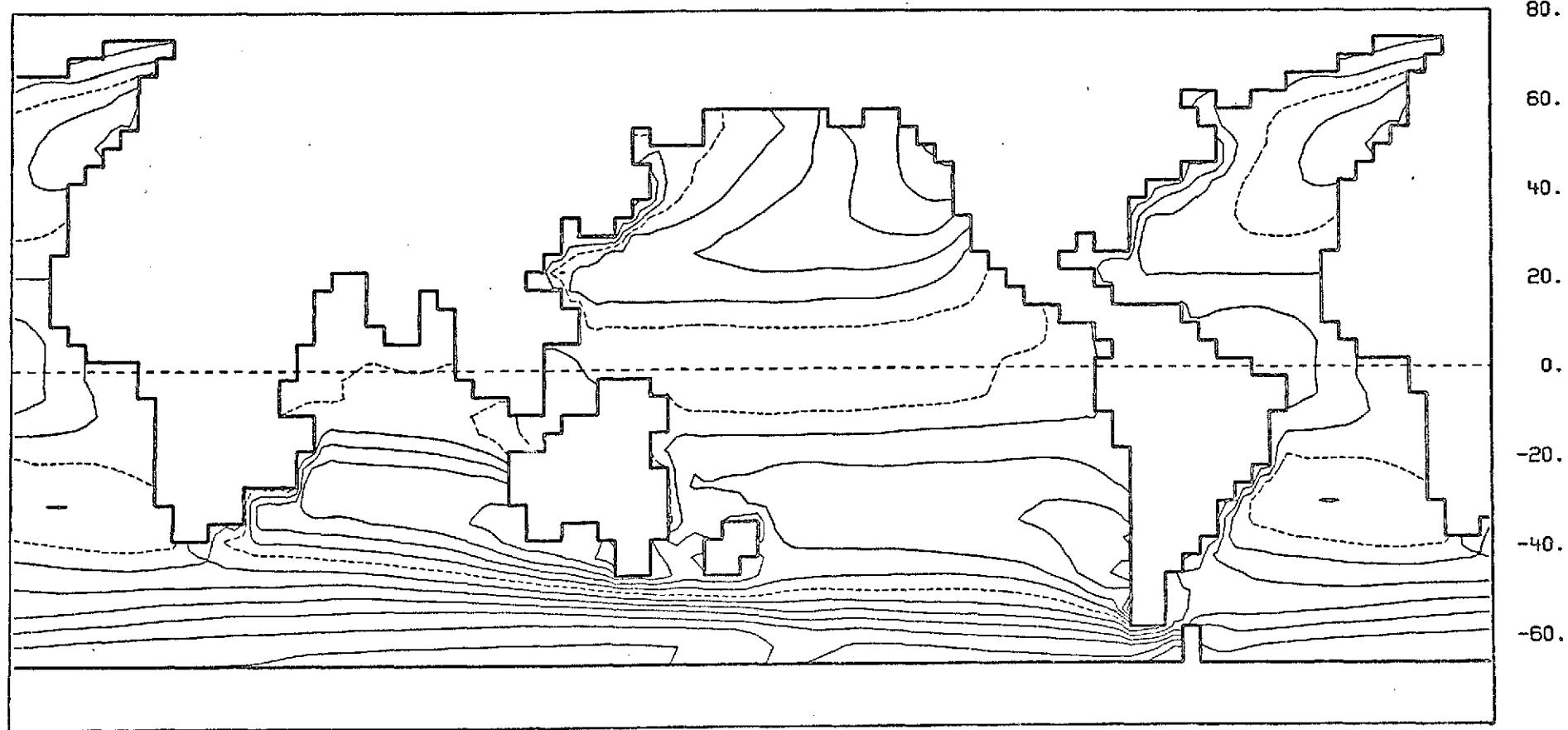
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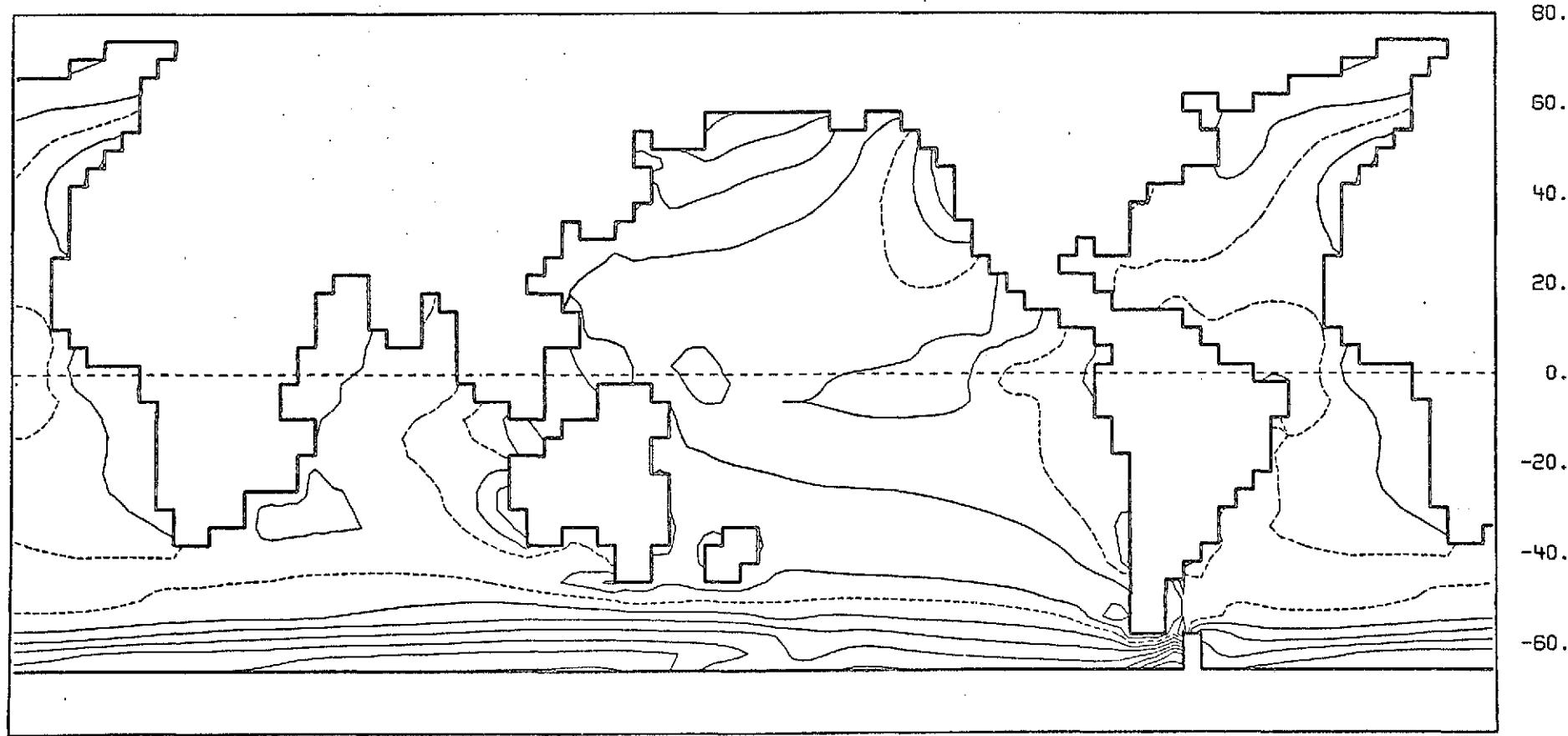
DASHED LINE = 7.0



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TEMPERATURE AT LEVEL 4 (DEG CENT)
CONTOUR INTERVAL = 0.5 (SOLID LINES)

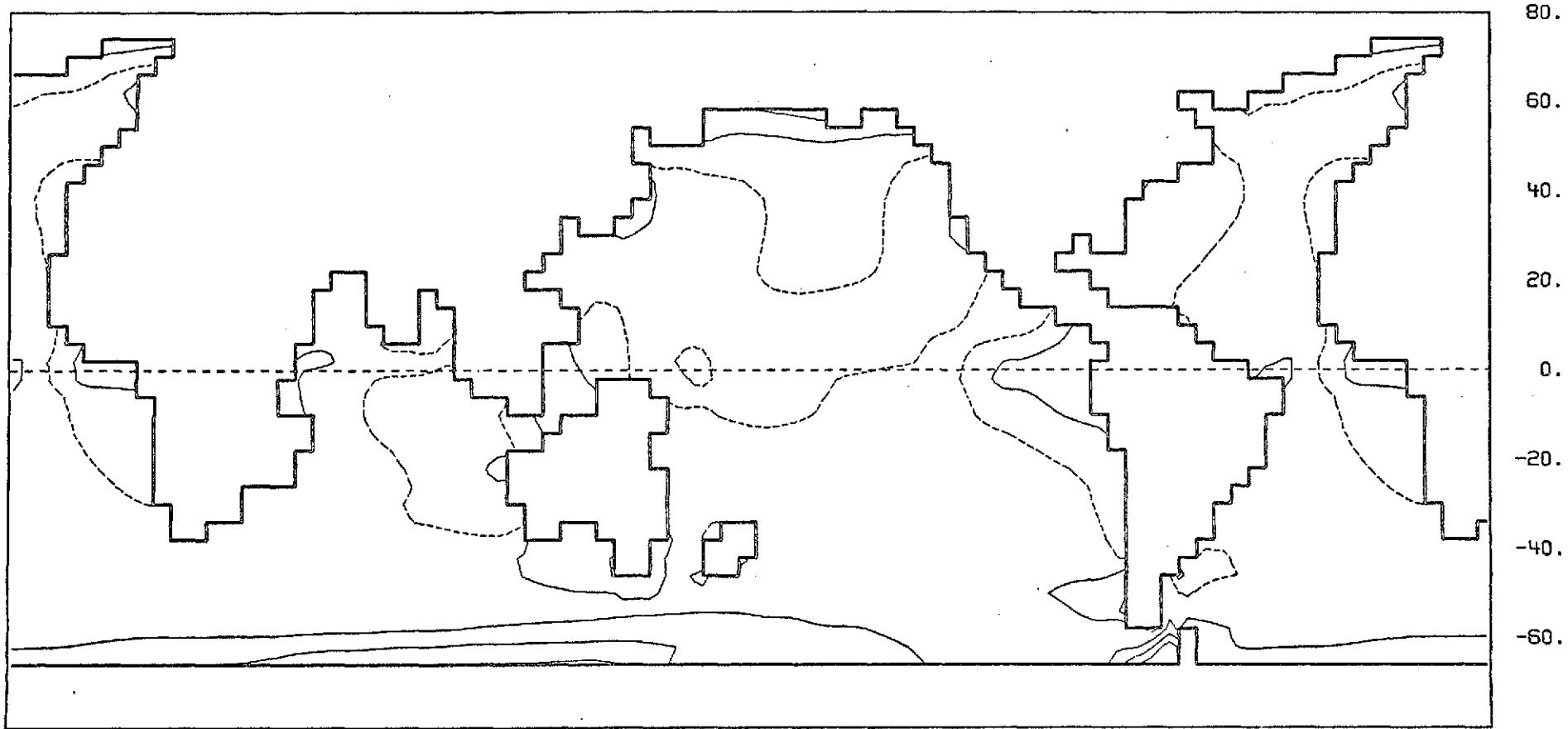
DASHED LINE = 3.5



EXPERIMENT S1
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TEMPERATURE AT LEVEL 5 (DEG CENT)
CONTOUR INTERVAL = 0.5 (SOLID LINES)

DASHED LINE = 2.0

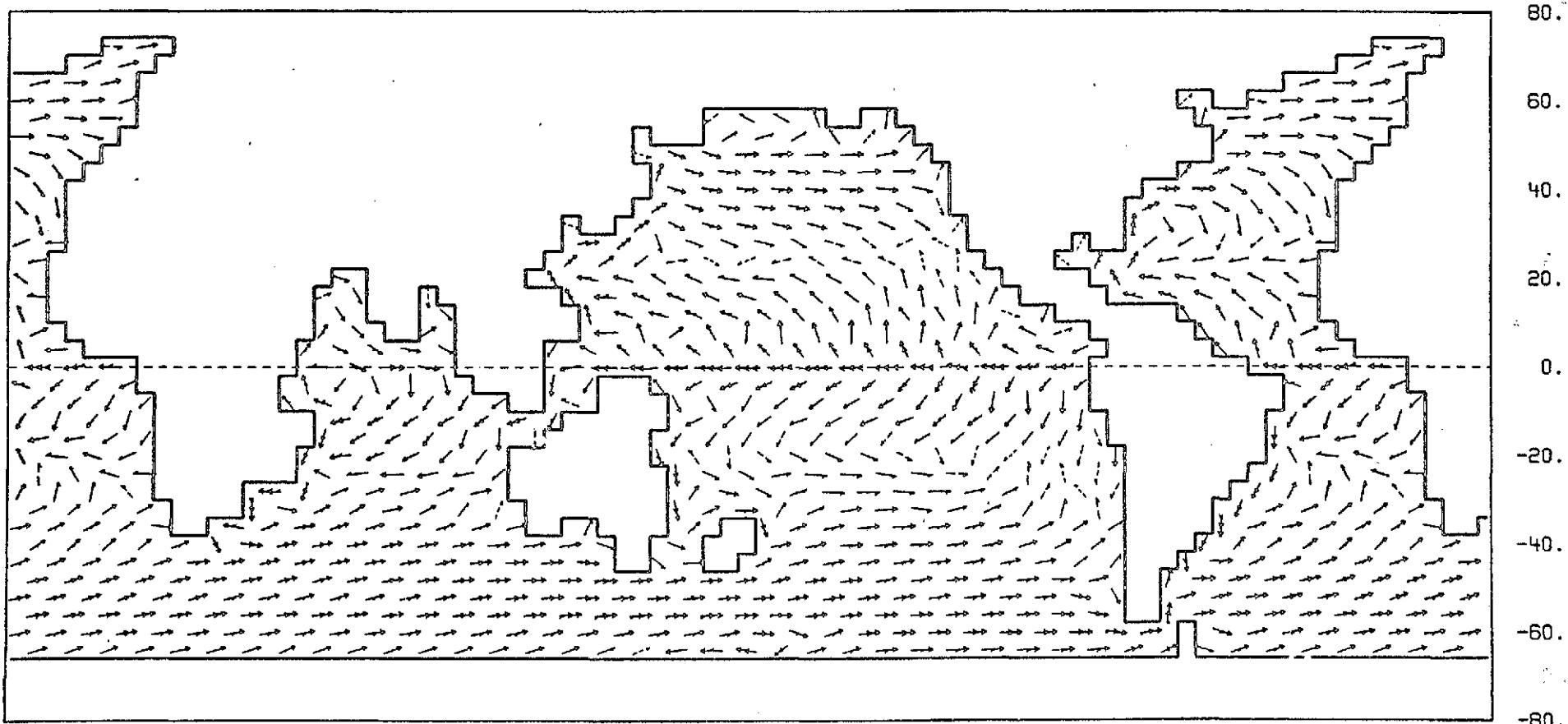


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 1 (CM/SEC)

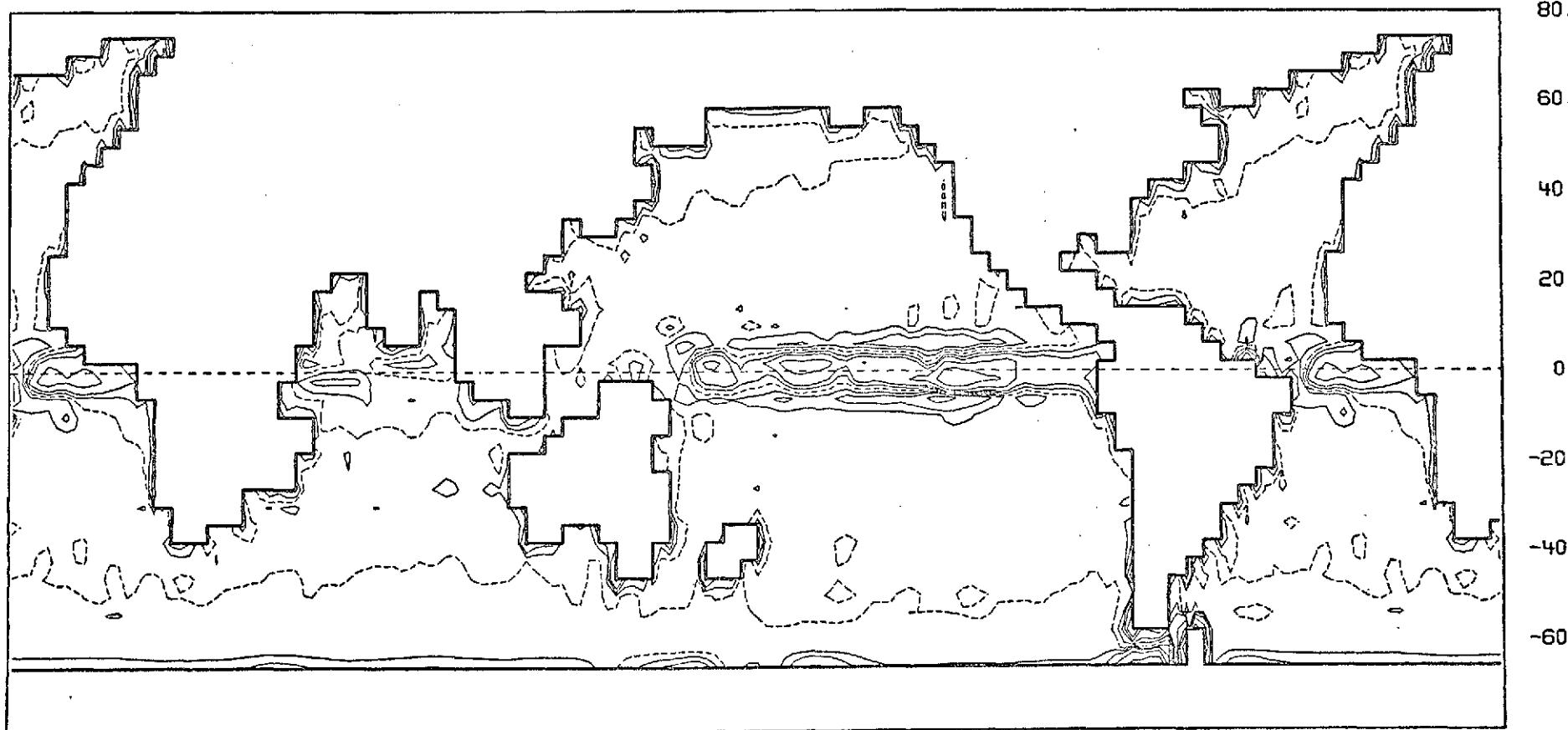
0.0 → 0.6 → 1.2 → 2.5 → 4.9 → 9.8 → 19.6 → 39.2 → 78.4



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VERTICAL VELOCITY AT LEVEL 1.5 (CM/DAY)
CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

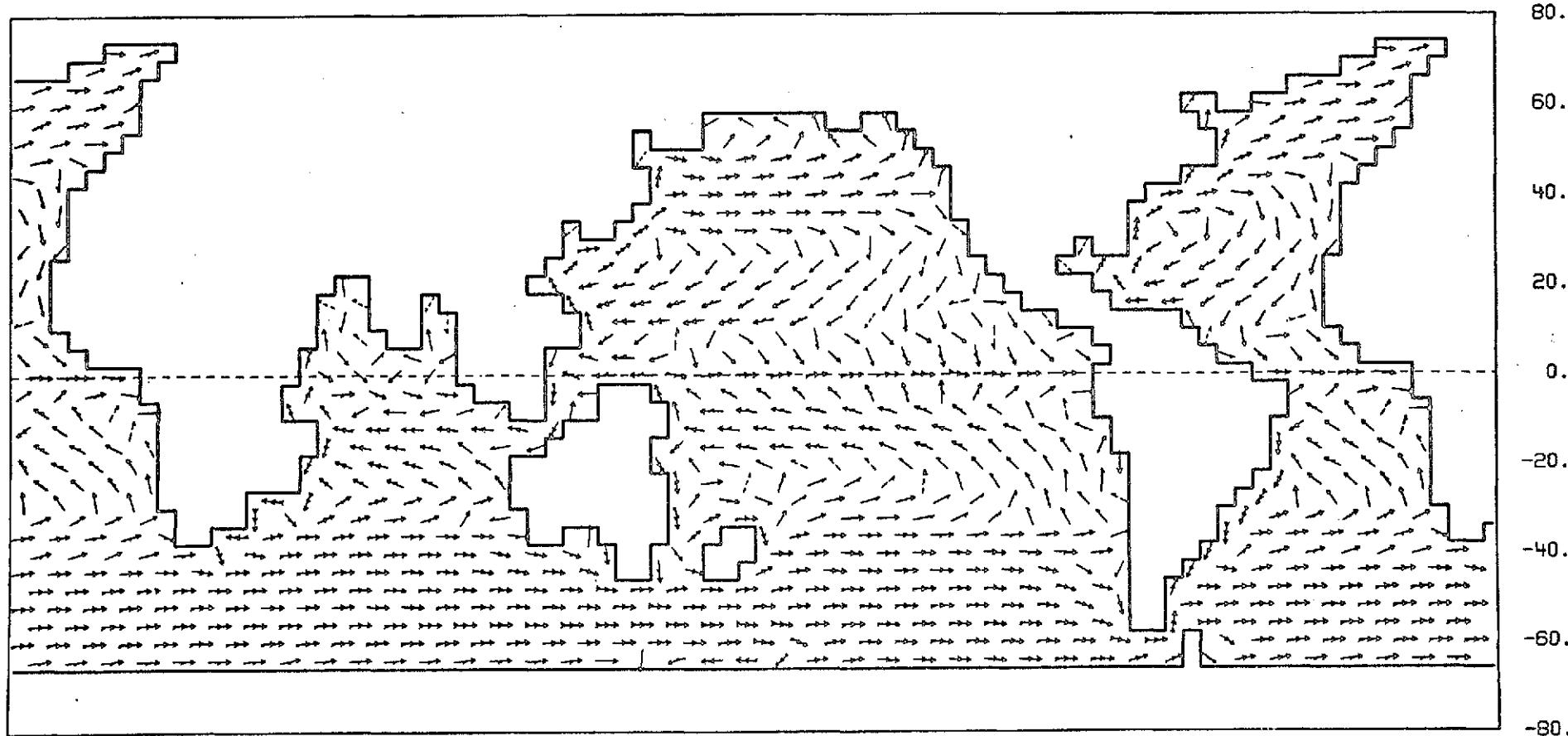
DASHED LINE = 0.0



EXPERIMENT S1
DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 2 (CM/SEC)

0.0 → 0.2 → 0.5 → 1.0 → 2.0 → 3.9 → 7.9 → 15.8 → 31.6



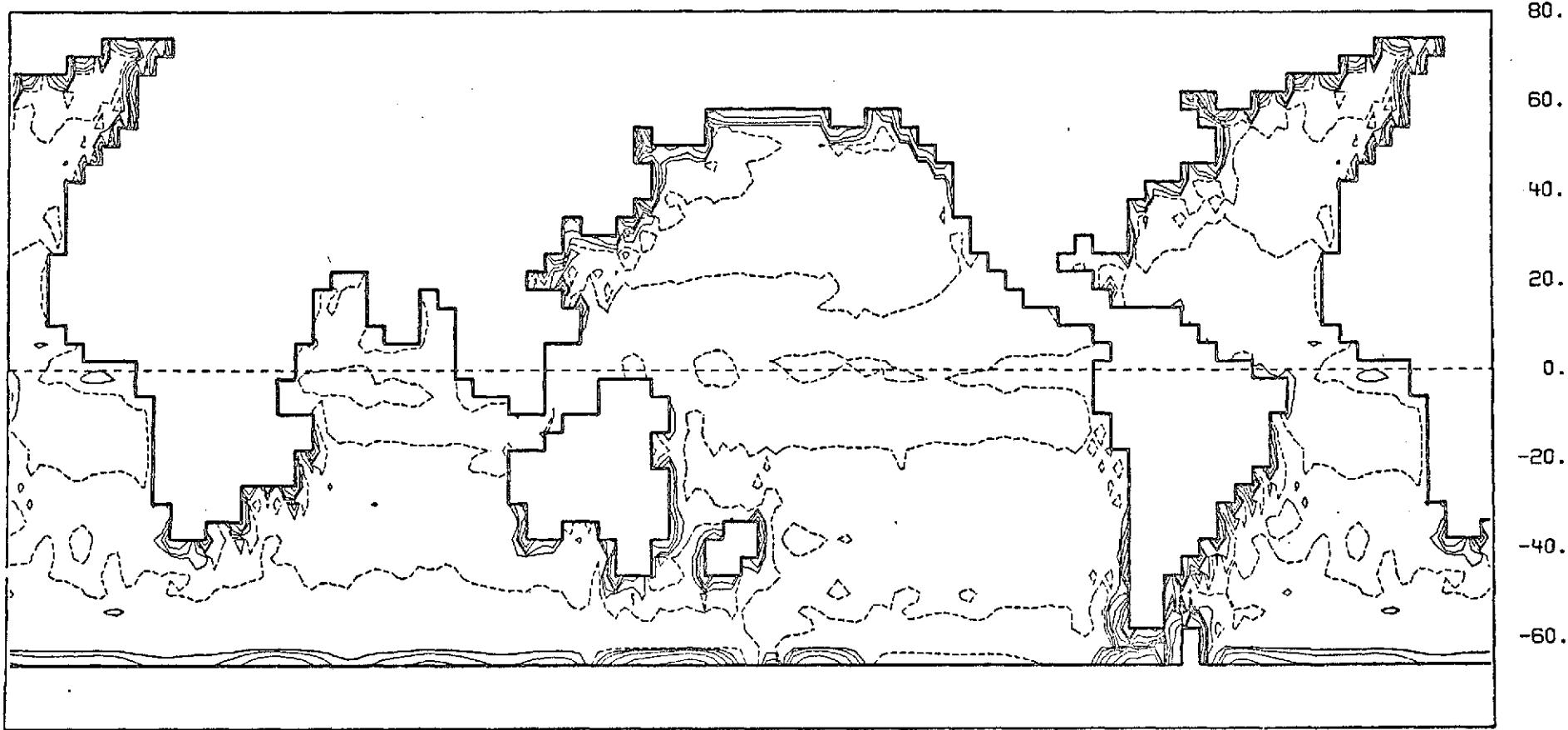
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VERTICAL VELOCITY AT LEVEL 2.5 (CM/DAY)

CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0

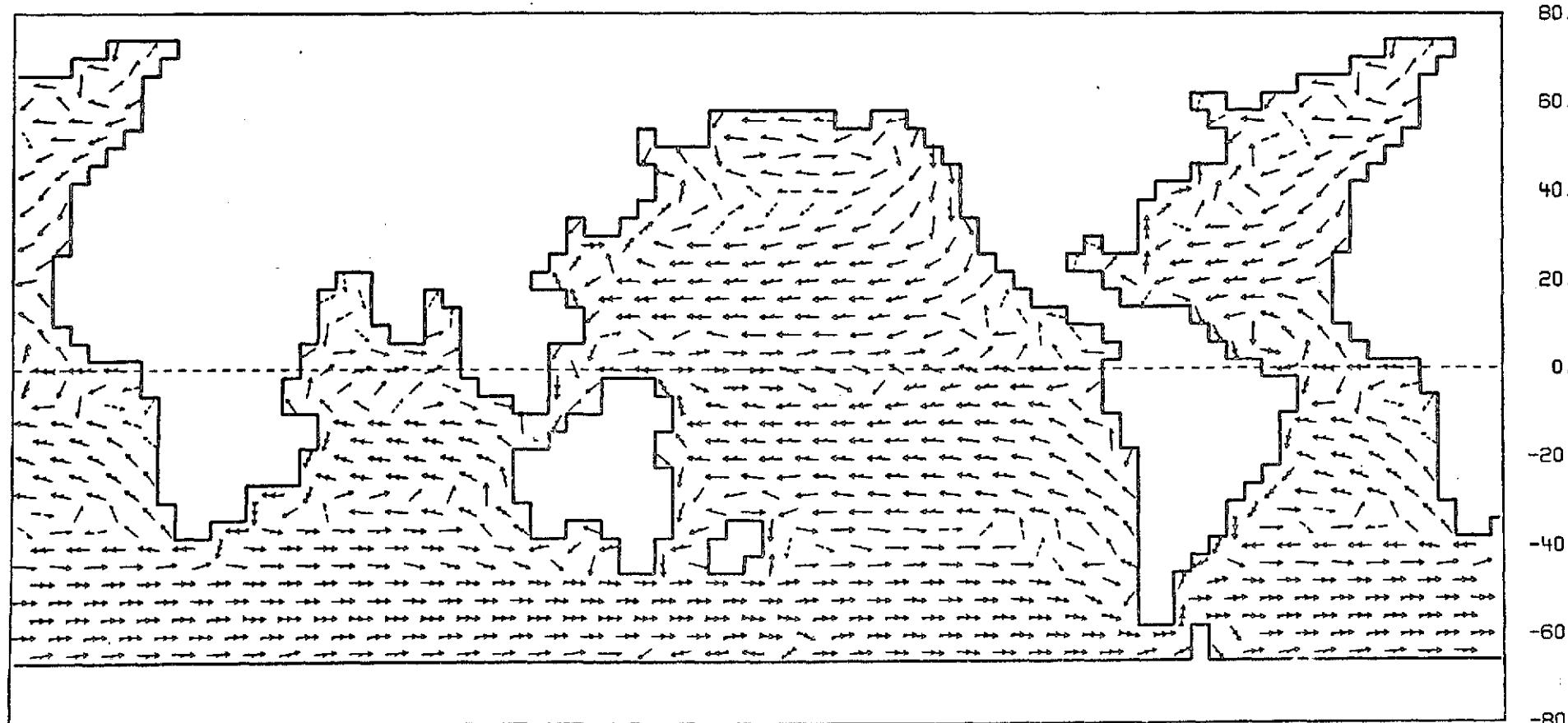


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 3 (CM/SEC)

0.0 → 0.2 → 0.4 → 0.7 → 1.4 → 2.9 → 5.8 → 11.6 → 23.2



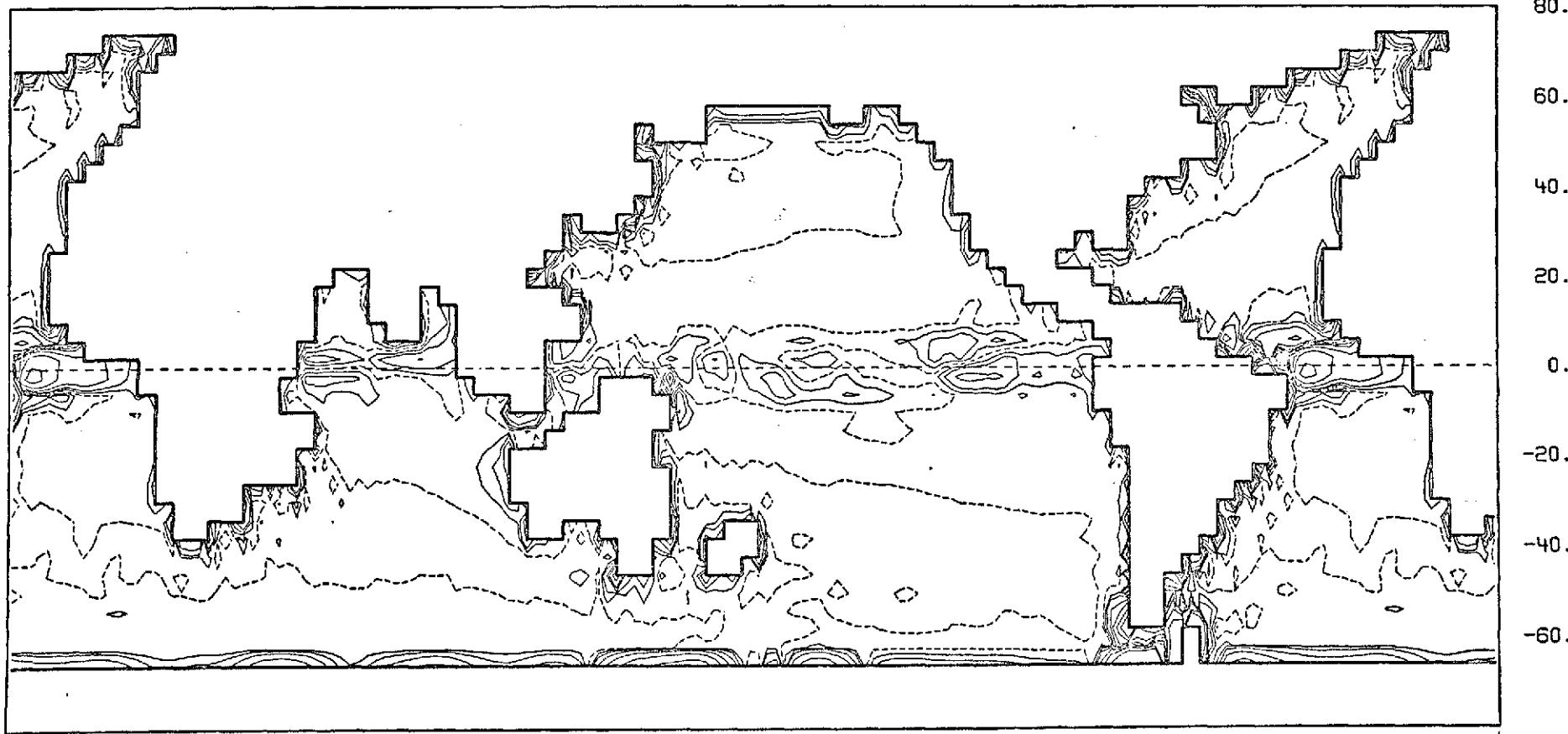
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VERTICAL VELOCITY AT LEVEL 3.5 (CM/DAY)

CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

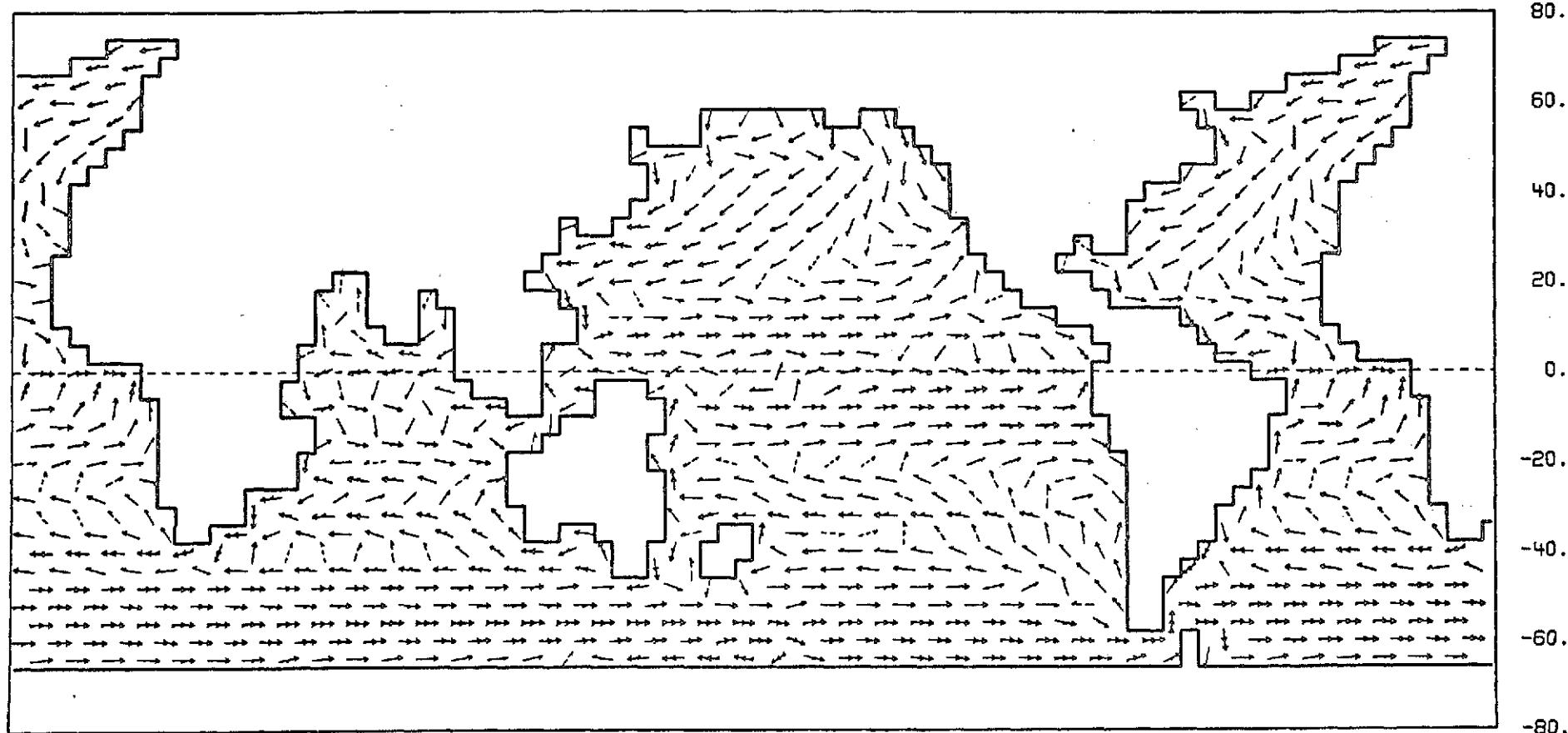
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HORIZONTAL VELOCITY AT LEVEL 4 (CM/SEC)

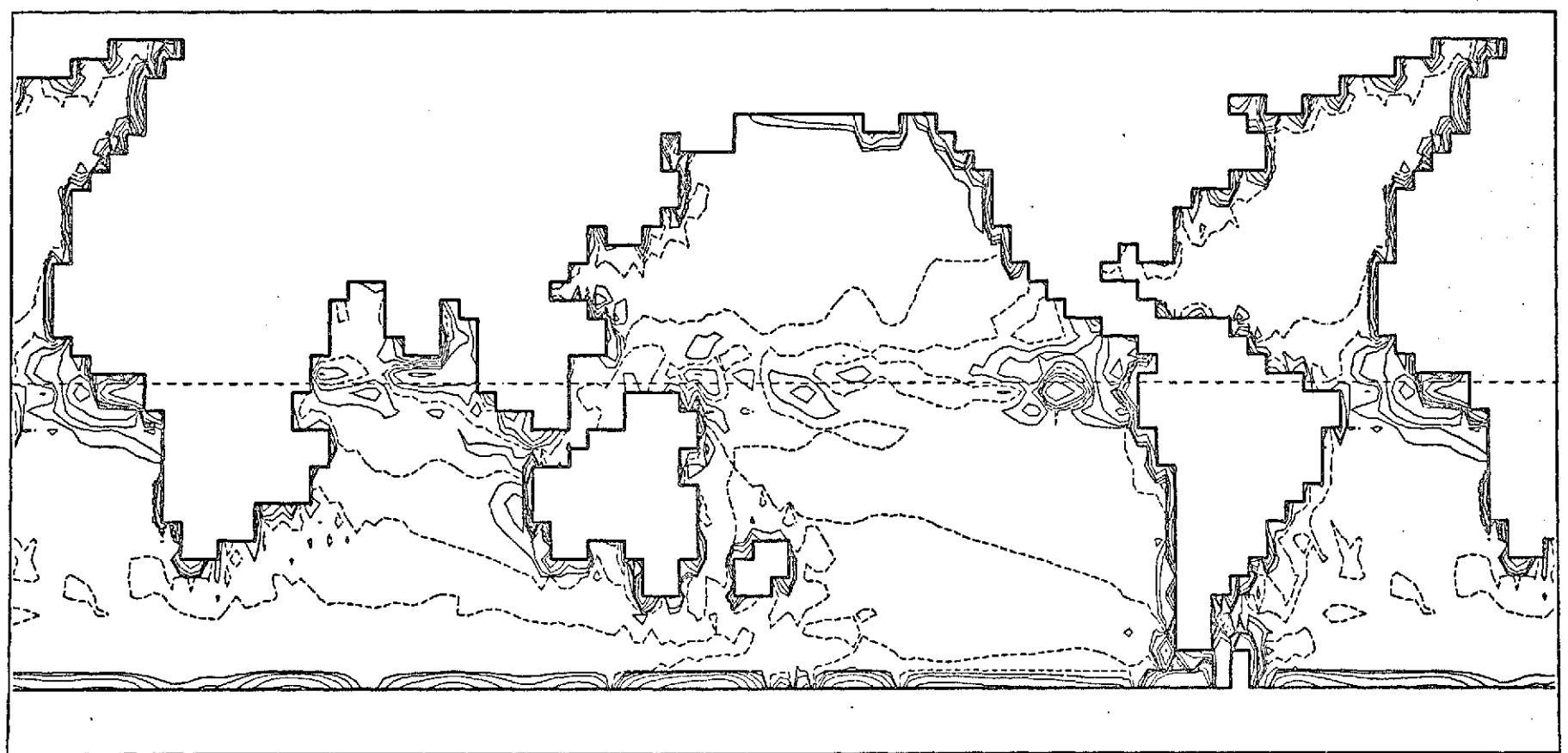
0.0 → 0.1 → 0.3 → 0.6 → 1.2 → 2.4 → 4.8 → 9.5 → 19.1



EXPERIMENT S1
DAY = 8773.7

VERTICAL VELOCITY AT LEVEL 4.5 (CM/DAY)
CONTOUR LINES 0, 25, 50, 100, 200, 400, 800

DASHED LINE = 0.0

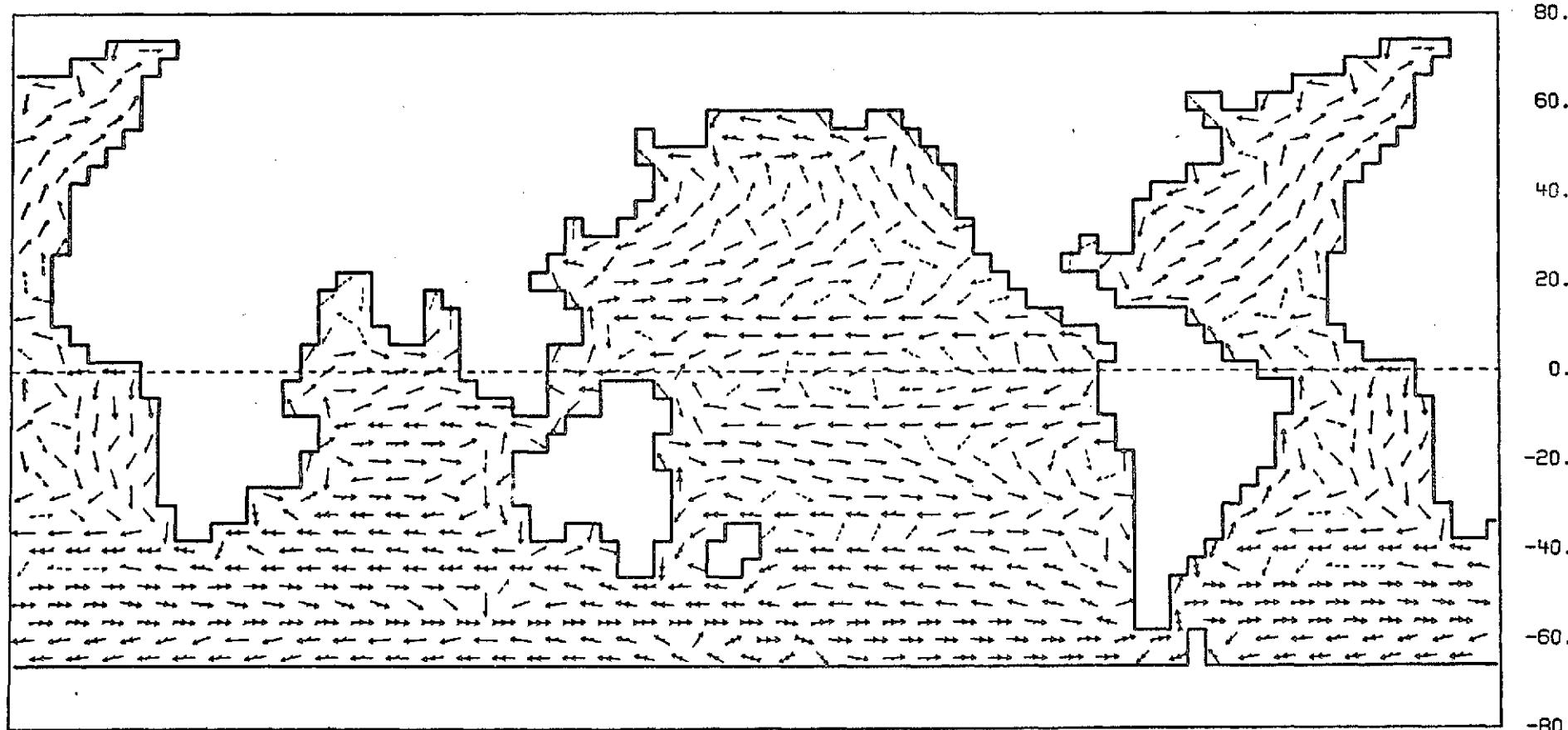


EXPERIMENT S1

DAY = 8773.7

HORIZONTAL VELOCITY AT LEVEL 5 (CM/SEC)

0.0 → 0.1 → 0.2 → 0.4 → 0.8 → 1.6 → 3.3 → 6.6 → 13.1



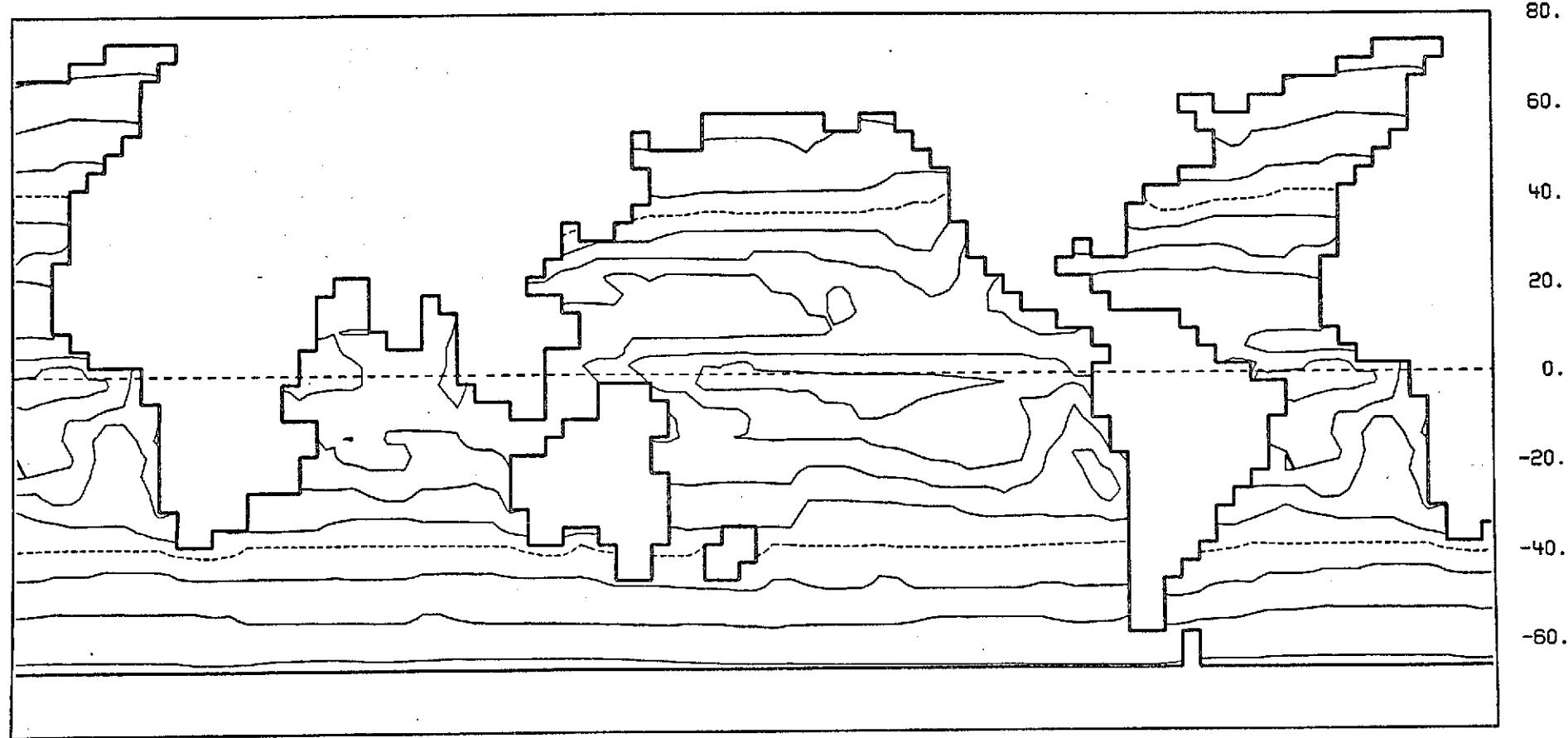
EXPERIMENT S1

DAY = 8773.7

SURFACE RADIATION FLUX (CAL/CM**2/DAY)

CONTOUR INTERVAL = 60.0

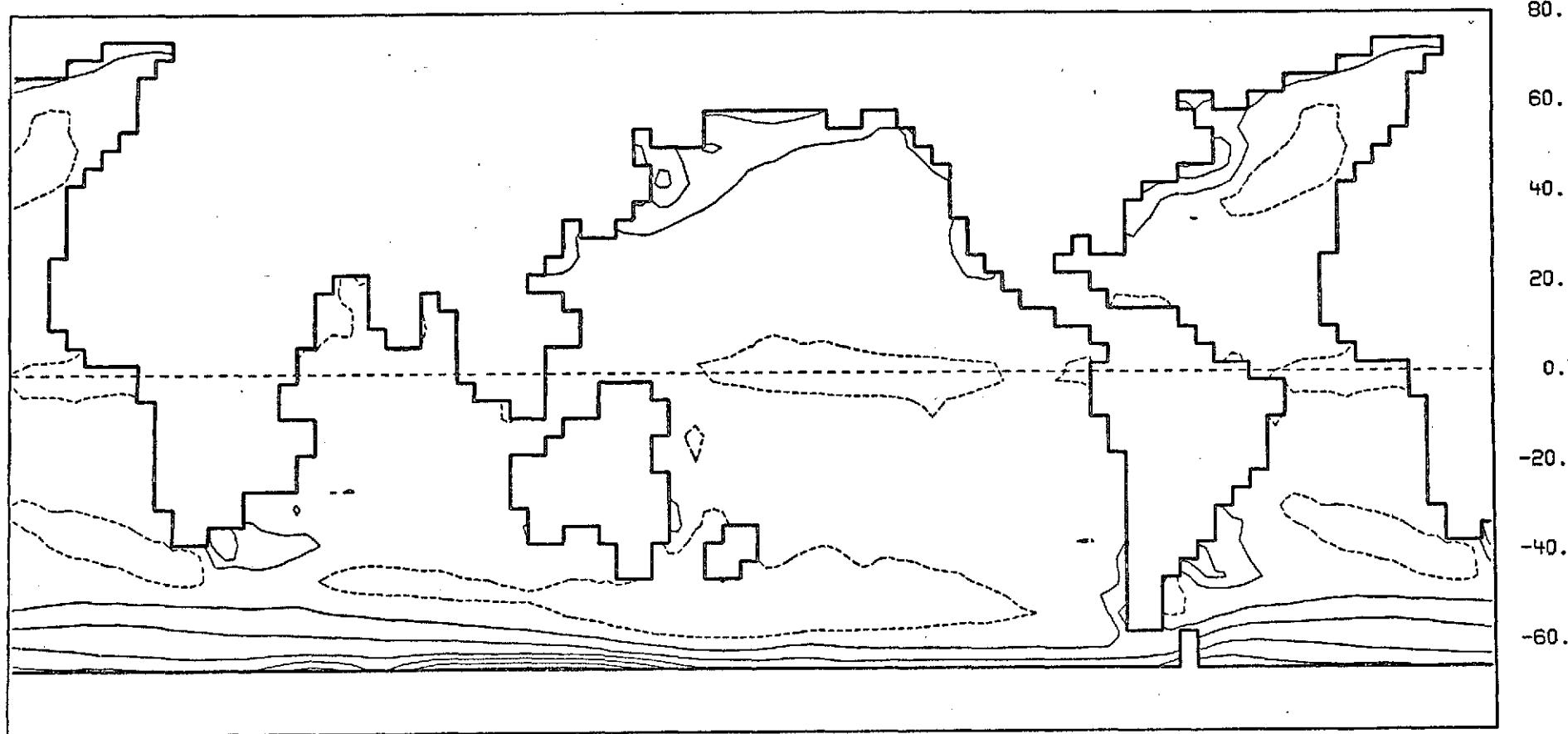
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EXPERIMENT S1
DAY = 8773.7

SURFACE SENSIBLE HEAT FLUX (CAL/CM**2/DAY)
CONTOUR INTERVAL = 60.0

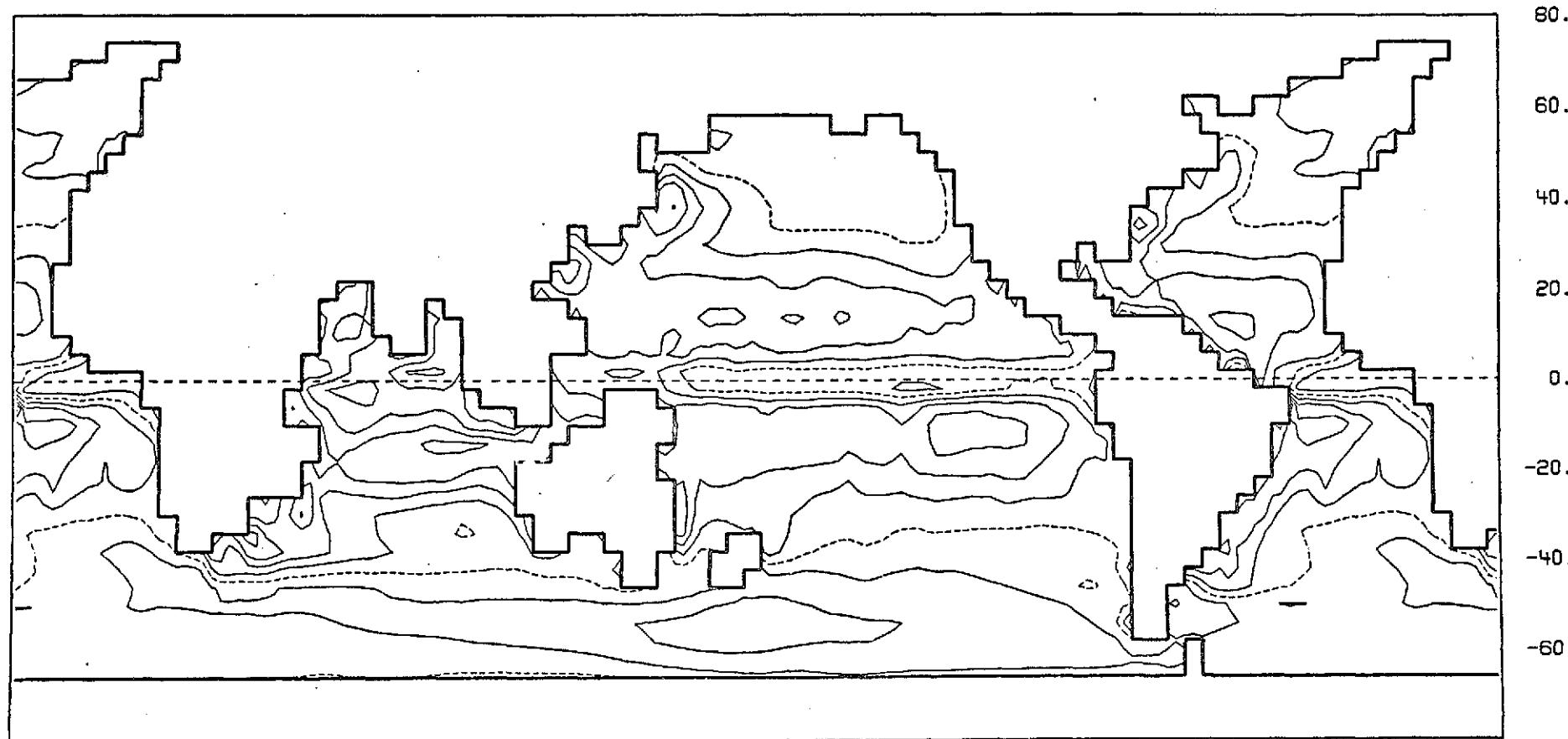
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EXPERIMENT S1
DAY = 8773.7

SURFACE LATENT HEAT FLUX (CAL/CM**2/DAY)
CONTOUR INTERVAL = 60.0

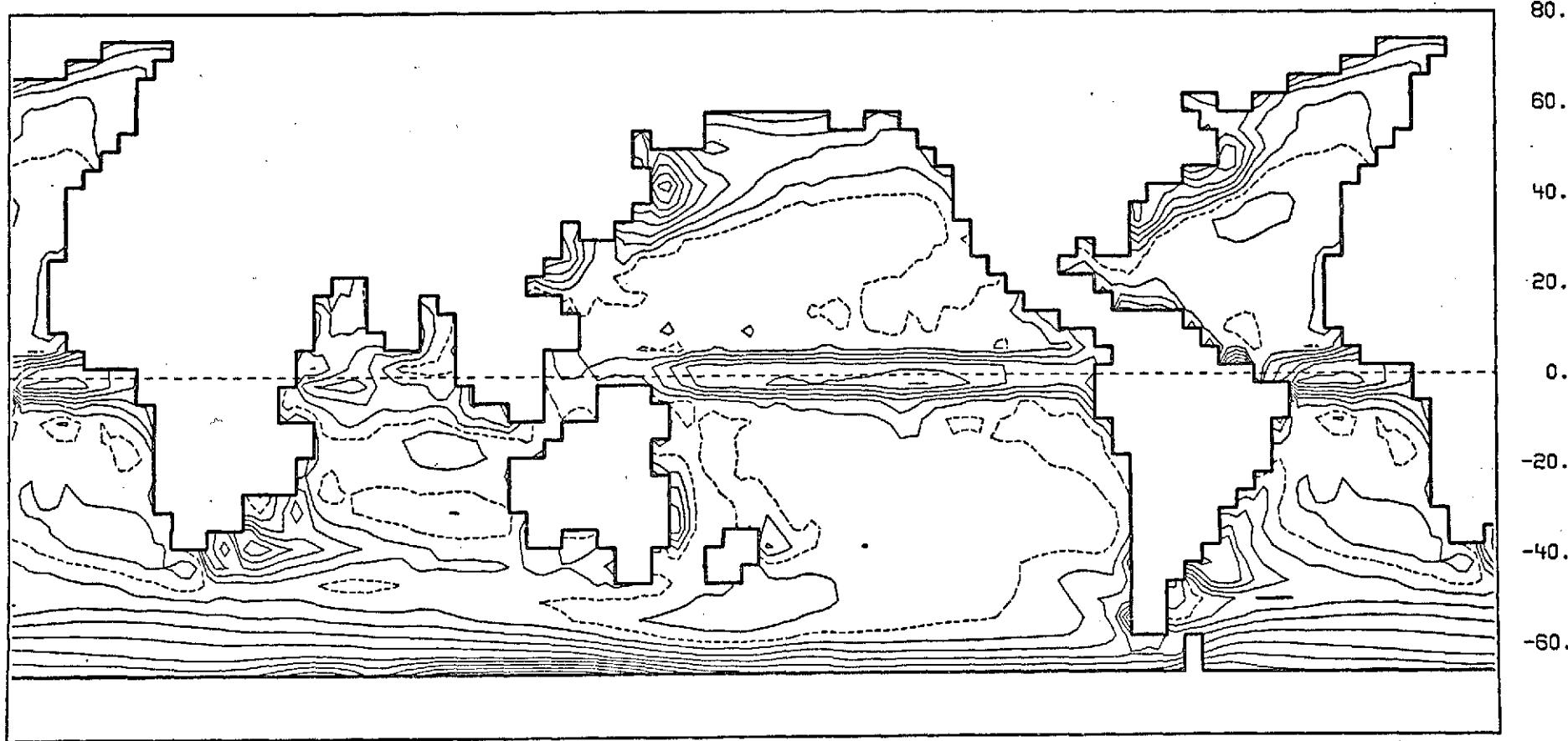
DASHED LINE = 180.0



EXPERIMENT S1
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TOTAL SURFACE HEAT FLUX (CAL/CM**2/DAY)
CONTOUR INTERVAL = 60.0

DASHED LINE = 0.0



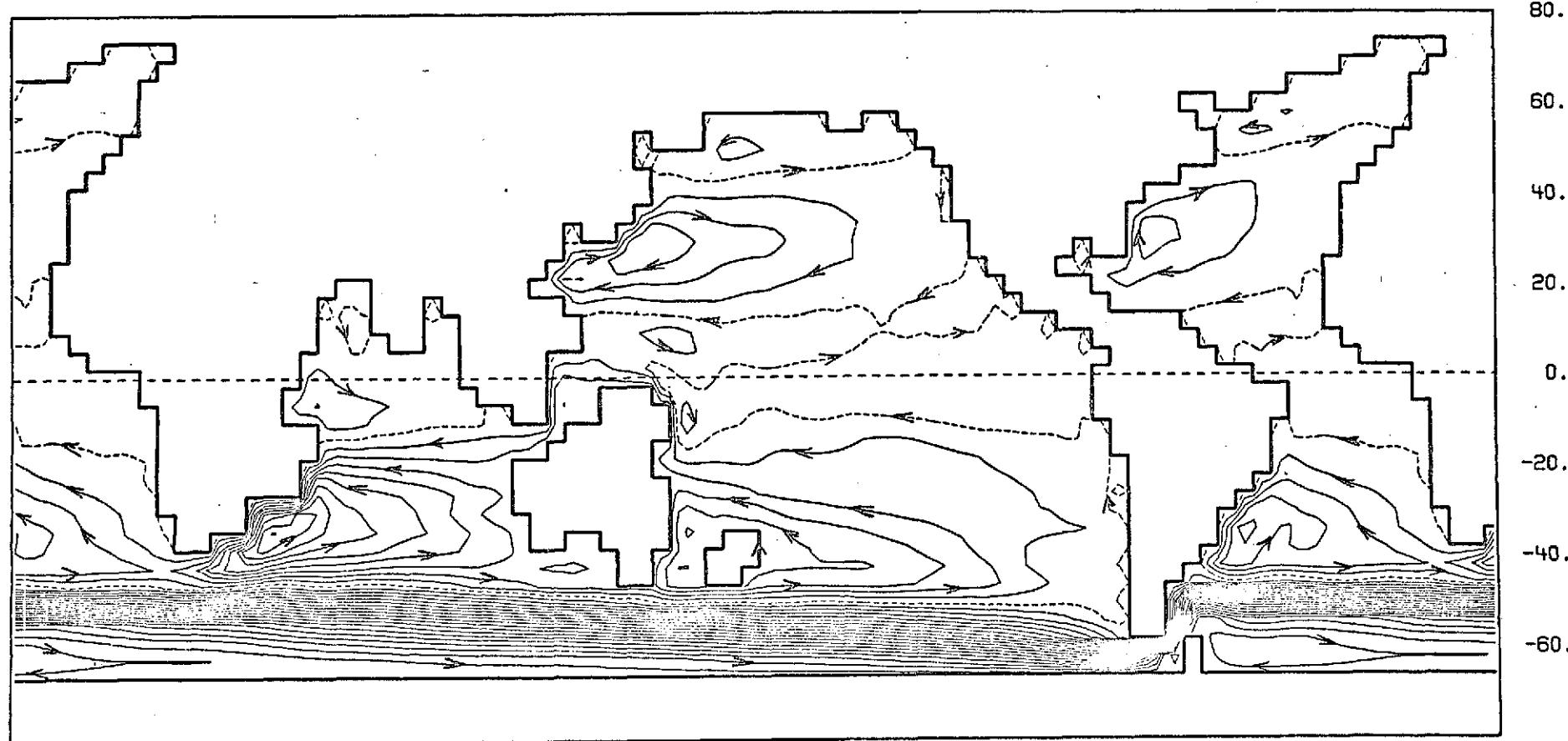
EXPERIMENT S1

DAY = 0.0

STREAM LINES OF HORIZONTAL TRANSPORT ($10^{12} \text{ CM}^3/\text{SEC}$)

CONTOUR INTERVAL = 10.0

DASHED LINE = 0.0



BAROTROPIC CIRCULATION IN A MULTI-CONNECTED GLOBAL OCEAN

MPP=0 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER POINTS,
 =1 IF ONE OF THE FOUR NEAREST SURROUNDING POINTS IS ON THE
 COAST OF THE MAIN LANDMASS (AFRICA, EUROPE, ASIA),
 =3 INSIDE THE ANTARCTICA,
 =30 ON THE COAST OF THE ANTARCTICA,
 =4 INSIDE AUSTRALIA,
 =40 ON THE COAST OF AUSTRALIA,
 =5 INSIDE NEWZEALAND,
 =50 ON THE COAST OF NEWZEALAND.

MULTIPLY THE STREAM FUNCTION VALUES BY R*H (R=EARTH'S
 RADIUS, H=OCEAN DEPTH) TO GET THE STREAM FUNCTION VALUES
 FOR THE VOLUME TRANSPORT (INTEGRAL OF THE HORIZONTAL VELOCITY
 OVER THE WHOLE DEPTH).

MQQ=1 FOR THE WATER POINTS,
 =2 FOR THE MAIN LAND MASS,
 =3 FOR THE ANTARCTICA,
 =4 FOR AUSTRALIA,
 =5 FOR NEWZEALAND.

THE SUBROUTINE HAJIME SPECIFY THE SHAPE OF THE OCEAN (MPP AND
 MQQ), THE WIND STRESS TO COMPUTE ITS CURL AND OTHER CONSTANTS
 AS WELL AS THE INITIAL FIELD OF THE STREAM FUNCTION.

THE SUBROUTINE RESID GIVES THE CHANGE OF THE SUM OF THE
 RESIDUALS (RES) AT EACH SEPARATE LAND MASS WHICH TAKES PLACE
 BY THE UNIT INCREASE OF THE STREAM FUNCTION AT EACH SEPARATE
 LAND MASS POINT, JUST AS IN CASE OF THE BLCK RELAXATION.

F AND G DENOTE THE STREAM FUNCTION AT TIME STEP N+1, N,
 RESPECTIVELY, XU, XV, U, AND V THE BAROTROPIC COMPONENTS AT TIME
 STEPS N+1, N, RESPECTIVELY.

WIND STRESS CURL=-TW/(2.0*Y*X(J))/R*H

X, XM, Y=GRID SIZE

AH=COEFFICIENT OF EDDY VISCOSITY

DT IS THE TIME STEP.

H IS THE OCEAN DEPTH. CD IS THE TIME (DAY).

E IS THE WORKING SPACE FOR RELAXATION.

IM DENOTES THE EASTERNMOST POINTS TO BE SWEPT. (EX. 146)

JM DENOTES THE NORTHERNMOST PONTS TO BE SWEPT.

THE BACKWARD DIFFERENCING SCHEME IN TIME APPLIES EVERY MAT
 TIME STEPS. MATS CONTROLS THE SWITCHING FRCM THE LEAP-FROG TO
 BACKWARD OF FROM THE BACKWARD TO LEAP-FROG SCHEMES.

PRINTING IS DONE EVERY NPRINT TIME STEPS.

WRINTING IN MAGNETIC TAPE IS DONE EVERY NTAPE TIME STEPS.

WHEN (IN) EQUALS ONE, THE IMAG-TH RECORD IN THE MAGNETIC TAPE
 IS PICKED UP, AND THE INTEGRATION GOES ON UNTIL NN=NEND.

REL=RELAXATION ACCURACY

WIND STRESS CURL=-TW(I,J)*H (DEPTH)/(2.0*Y*X(J)*RAD) RAD=
 RADIUS OF THE EARTH)

IND(1)=30 ANTARCTIC COAST

IND(2)=40 AUSTRALIA COAST

IND(3)=50 NEWZEALAND COAST

INDIN(1)=3 ANTARCTIC INLAND

INDIN(2)=4 AUSTRALIA INLAND

INDIN(3)=5 NEWZEALAND INLAND

FIGURE 1 EXPLAINS THE MEANING OF LX1, LX2, LY1 AND LY2.

X=LX1	***	X=LX2
Y=LY2	***	Y=LY2

 ** ISLAND
 **
 **
 **
 X=IX1 ** X=LX2
 Y=LY1 ** Y=LY1

FIG. 1

L, KA, KB SPECIFY THE STREAM FUNCTION POINTS TO BE SWEPT AND OTHER LAND POINTS TO BE SKIPPED.

FIGURE 2 EXPLAINS THEIR MEANINGS.

* POINT TO BE SWEPT

J=4 KA(1,J) ***KB(1,J) KA(2,J) ***KB(2,J) KA(3,J) ***KB(3,J)
 L(J)=3

FIG. 2

THE COMPUTATION STOPS IF THE ENERGY EXCEEDS A CERTAIN VALUE, OR IF THE NUMBER OF ITERATION IN RELAXATION EXCEEDS A CERTAIN VALUE. THESE VALUES ARE SPECIFIED IN THE PROGRAM. THEY SHOULD BE CHANGED IF NECESSARY.

THE COEFFICIENT OF THE OVER-RELAXATION IS GIVEN AT THE BEGINNING.

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COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),P(147,39),E(147,39),
IU(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3), DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
SOR=1.775
SOR=1.875
SOR=1.825
SOR=1.85
SOR1=SOR-1.0
READ(5,1000) IN
1000 FORMAT(I5)
IF(IN.EQ.1) GO TO 1001
CALL HAJIME
CALL RESID
CD=0.0
NN=0
MAG=0
GO TO 5555
1001 CONTINUE
READ(5,1000) IMAG
IF(IMAG.EQ.1) GO TO 77
DO 7 J=2,IMAG
READ(10)
7 CONTINUE
7 READ(10) XU,XV,F,G,U,V,TW,MPP,QQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
5555 CONTINUE
AH=1.0E9
AH=3.0E8
AR=AH/6.37E8/6.37E8
ARY=AR/Y
TUR C-MM 1

```

```

NN=0.0
READ(5,5) NEND, MAT, NPRINT, NTAPE, DT, REL
5 FORMAT(4I5, 2E15.7)
WRITE(6,6) IIMAG, NEND, DT, REL, AH, MAT, NTAPE, NPRINT
6 FORMAT(1H ,16 HTIME STEP FROM I5, 2X, 3H TO I5, 2X, 3HDT=E15.7, 2X, 4HREL
1=E15.7, 2X, 3H A H=E15.7, 2X, 4H MAT=I3/1H , 5HTAPE=I4, 5X, 6H PRINT=I4)
20 DAY=DT/0.864E5
MQQ(49,5)=1
MQQ(50,5)=1
MQQ(49,3)=3
MQQ(50,3)=3
39 NN=NN+1
CD=CD+DAY
NNN=(NN/MAT)*MAT
IF(NNN.EQ.NN) GO TO 25
MATS=0
DDT=DT
DO 1 J=3,JM
DO 2 I=1,IMP1
R=G(I,J)
G(I,J)=F(I,J)
F(I,J)=R
2 CONTINUE
1 CONTINUE
GO TO 26
25 MATS=1
DDT=DT*0.5
DO 42 J=3,JM
DO 43 I=1,IMP1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
G(I,J)=F(I,J)
43 CONTINUE
42 CONTINUE
26 CONTINUE
DO 30 J=3,JM
JP1=J+1
JM1=J-1
JM2=J-2
XMJ=XM(J)
XM1=XM(JM1)
C1=Y/XMJ
S1=Y/XM1
CB=X(JP1)/Y
CS=X(J)/Y
B=X(JM1)/Y
BETJ=BET(J)*CCY
LJ=L(J)
DO 31 LL=1,LJ
II=KA(LL,J)
MM=KB(LL,J)
DO 310 I=II,MM
IP1=I+1
IM1=I-1
IM2=I-2
UIJ=U(I,J)
VIJ=V(I,J)
UP1J=U(IP1,J)
UM1J=U(IM1,J)
UIP1=U(I,JP1)
UM1P1=U(IM1,JP1)
UIM1=U(I,JM1)
UM1M1=U(IM1,JM1)
UP1M1=U(IP1,JM1)
UIM2=U(I,JM2)
UM1M2=U(IM1,JM2)
VIM2=V(I,JM2)

```

```

UM2J=U(IM2,J)
VM2J=V(IM2,J)
UM1M2=U(IM1,JM2)
VM1M2=V(IM1,JM2)
UM2M1=U(IM2,JM1)
VM2M1=V(IM2,JM1)
VP1J=V(IP1,J)
VM1J=V(IM1,J)
VIP1=V(I,JP1)
VIM1=V(I,JM1)
VM1P1=V(IM1,JP1)
VM1M1=V(IM1,JM1)
VP1M1=V(IP1,JM1)
MP=MPP(I,J)
IF(MP.EQ.0) GO TO 304
IF(MP.EQ.30) GO TO 304
IF(MP.EQ.50) GO TO 304
IF(MQQ(IP1,J).NE.2) GO TO 27
UP1J=-UIJ
VP1J=-VIJ
27 IF(MQQ(I,JP1).NE.2) GO TO 271
UIP1=-UIJ
VIP1=-VIJ
271 IF(MQQ(IM1,JP1).NE.2) GO TO 272
UM1P1=-UM1J
VM1P1=-VM1J
272 IF(MQQ(IM2,J).NE.2) GO TO 28
UM2J=-UM1J
VM2J=-VM1J
28 IF(MQQ(IM2,JM1).NE.2) GO TO 29
UM2M1=-UM1M1
VM2M1=-VM1M1
29 IF(MQQ(IM1,JM2).NE.2) GO TO 291
UM1M2=-UM1M1
VM1M2=-VM1M1
291 IF(MQQ(I,JM2).NE.2) GO TO 292
UIM2=-UIM1
VIM2=-VIM1
292 IF(MQQ(IP1,JM1).NE.2) GO TO 303
UP1M1=-UIM1
VP1M1=-VIM1
303 CONTINUE
304 DF=-BET J      *(XV(I,J)+XV(IM1,J)+XV(IM1,JM1)+XV(I,JM1))*0.25
SS=(C1*(UM1J+UIJ-UM2J-UP1J)-(UIP1-UIJ+UM1P1-UM1J)*CB+2.0*CS*
1(UIJ-UIM1+UM1J-UM1M1)+S1*(UP1M1+UM2M1-UIM1-UM1M1)-(UIM1-UIM2+UM1M1
2-UM1M2)*B)*ARY+TW(I,J)+DF
DF=CS*(VIJ-VM1J+VM1M1)
SS= AR/XMJ*(C1*(-3.0*(VIJ-VM1J)+VP1J-VM2J)-DF
1+(VIP1-VIJ-VM1P1+VM1J)*CB)+AR/XM1*(S1*(3.0*(VM1M1-VIM1)+VP1M1
2-VM2M1)+(VM1M1-VM1M2-VIM1+VIM2)*B+DF)+SS
4 E(I,J)=-SS*DDT
310 CONTINUE
31 CONTINUE
E(2,J)=E(IM,J)
E(IMP1,J)=E(3,J)
30 CONTINUE
IP=0
37 IP=IP+1
***ISLANDS
MAR=0
C*****ANTARCTICA
C*****NEWZEALAND
C*****AUSTRALIA
DO 5021 K=1,3
RESK=RES(K)
MP=IND(K)

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MPMP=INDIN(K)
II=LX1(K)
IG=LX2(K)
IM2=LY1(K)
JM2=LY2(K)
R=0.0
DO 5016 J=IM2,JM2
DO 5015 I=II,IG
IF(MPP(I,J).NE.MP) GO TO 5015
R=R+E(I,J)
5015 CONTINUE
5016 CONTINUE
IF(ABS(R).LE.REL) GO TO 5021
DF=-R/RESK
MAR=MAR+1
IF(K.EQ.1) IM2=2
DO 5022 J=IM2,JM2
JP1=J+1
JM1=J-1
CS=Y/X(J)
CB= 2.0*(CS+1.0/CS)
SS=X(JP1)/Y
C1=X(JM1)/Y
DO 5023 I=II,IG
MPPIJ=MPP(I,J)
MMMM=(MPPIJ-MP)*(MPPIJ-MPMP)
IF(MMM.ME.0) GO TO 5023
F(I,J)=F(I,J)+DF
IM1=I-1
IP1=I+1
CCC=DF*CS
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
E(IP1,J)=E(IP1,J)+CCC
E(IM1,J)=E(IM1,J)+CCC
E(I,J)=E(I,J)-CB*DF
5023 CONTINUE
5022 CONTINUE
IF(K.EQ.2) GO TO 5021
IF(K.EQ.1) GO TO 5024
DO 5026 J=8,12
E(2,J)=E(IM,J)
5026 CONTINUE
GO TO 5021
5024 CONTINUE
E(IMP1,5)=E(3,5)
E(2,5)=E(IM,5)
CCC=DF*Y/X(4)
E(3,4)=E(3,4)+CCC
E(IM,4)=E(IM,4)+CCC
E(IMP1,4)=E(3,4)
E(2,4)=E(IM,4)
5021 CONTINUE
C*****NEWZEALAND
C*****ANTARCTICA
DO 32 J=4,JM
JM1=J-1
JP1=J+1
XJ=X(J)
CS=Y/XJ
SS=X(JP1)/Y
C1=X(JM1)/Y
CB=2.0*(CS+XJ/Y)
LJ=L(J)
DO 33 LL=1,LJ
TT=RA(LL,J)

```

```

      DO 330 I=II,MM
      IF(MPP(I,J).GE.3) GO TO 330
      R=E(I,J)
      IF(ABS(R).LE.REL) GO TO 330
      MAR=MAR+1
      DF=R/CB*SOR
      E(J,J)=-R*SOR
      F(I,J)=F(I,J)+DF
      IP1=I+1
      CCC=DF*CS
      E(IP1,J)=E(IP1,J)+CCC
      IM1=I-1
      E(IM1,J)=E(IM1,J)+CCC
      E(I,JP1)=E(I,JP1)+SS*DF
      E(I,JM1)=E(I,JM1)+C1*DF
      IF(I.NE.3) GO TO 331
      E(IMP1,JP1)=E(3,JP1)
      E(IMP1,JM1)=E(3,JM1)
      E(IMP1,J)=E(3,J)
      E(IM,J)=E(2,J)
      GO TO 330
331 IF(I.NE.IM) GO TO 332
      E(2,J)=E(IM,J)
      E(2,JP1)=E(IM,JP1)
      E(2,JM1)=E(IM,JM1)
      E(3,J)=E(IMP1,J)
      GO TO 330
332 IF(I.NE.4) GO TO 333
      E(IMP1,J)=E(3,J)
      GO TO 330
333 IF(I.NE.IMM1) GO TO 330
      E(2,J)=E(IM,J)
330 CONTINUE
33 CONTINUE
32 CONTINUE
      IF(MAR.EQ.0) GO TO 36
      IF(IP.GT.1000) GO TO 1112
      IF(IP.NE.1) GO TO 37
      WRITE(6,38) IP,MAR
38 FORMAT(1H ,7X,6HKAI SU=I5,5X,12HTEN NO KAZU=I5)
      GO TO 37
36 EN=0.0
      WRITE(6,38) IP,MAR
      DO 70 J=3,JM
      F(1,J)=F(IMM1,J)
      F(2,J)=F(IM,J)
      F(IMP1,J)=F(3,J)
70 CONTINUE
      DO 23 J=3,JM
      JM1=J-1
      JP1=J+1
      XMJ=XM(J)*2.0
      DF=XMJ*Y4
      LVJ=LV(J)
      DO 24 LJ=1,LVJ
      II=LA(LJ,J)
      IG=LB(LJ,J)
      DO 244 I=II,IG
      IP1=I+1
      U(I,J)=XU(I,J)
      V(I,J)=XV(I,J)
      XU(I,J)=
1          (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
      XV(I,J)=
1          (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ

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```

LN=EN+DF*(XU(1,J)+Z+KV(1,J)*Z)
244 CONTINUE
24 CONTINUE
XU(IMP1,J)=XU(3,J)
XV(IMP1,J)=XV(3,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)
XU(2,J)=XU(IM,J)
XV(2,J)=XV(IM,J)
XU(1,J)=XU(IMM1,J)
XV(1,J)=XV(IMM1,J)
U(2,J)=U(IM,J)
V(2,J)=V(IM,J)
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
23 CONTINUE
WRITE(6,34) NN,CD,EN,F(1,3)
34 FORMAT(1H ,5HSTEP=I5,5X,5HTIME=E15.7,5X,7HENERGY=E15.7,5X,4HACC=F7
1.4)
IF(EN.GT.5.0E1) GO TO 1111
IF(NN.GE.NEND) GO TO 88
IF(MATS.NE.0) GO TO 10
IF(NN.NE.((NN/NTAPE)*NTAPE)) GO TO 9
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MOO,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
9 IF(NN.EQ.((NN/NPRINT)*NPRINT)) GO TO 88
10 ENN=EN
IF(MATS.EQ.0) GO TO 39
MATS=MATS+1
IF(MATS.EQ.3) GO TO 46
DO 44 J=3,JM
DO 45 I=1,IMP1
F(I,J)=G(I,J)
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
45 CONTINUE
44 CONTINUE
GO TO 26
46 DO 47 J=3,JM
DO 48 I=1,IMP1
R=F(I,J)
F(I,J)=G(I,J)
G(I,J)=R
48 CONTINUE
47 CONTINUE
DO 49 J=3,JM
JP1=J+1
XMJ=XM(J)*2.0
LVJ=LV(J)
DO 55 LJ=1,LVJ
II=LA(LJ,J)
IG=LB(LJ,J)
DO 550 I=II,IG
IP1=I+1
U(I,J)=
1 (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
V(I,J)=
1 (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ
550 CONTINUE
55 CONTINUE
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
U(2,J)=U(IM,J)

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```

V(2,J)=V(1H,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)

49 CONTINUE
MATS=0
NN=NN+1
DDT=DT
NNT=NNT+1
CD=CD+DAY
GO TO 39

88 K=1
MP=-1
613 MP=MP+1
MM=K-MP
IG=18*MP+3
IF(MM.EQ.0) GO TO 614
II=IG+17
GO TO 615

614 II=38
615 WRITE(6,701)
701 FORMAT(1H0,15HSTREAM FUNCTION)
DO 702 J=1,IMP1
WRITE(6,703) J,(F(J,I),I=IG,II)
703 FORMAT(1H ,I3,1X,18F7.4)
702 CONTINUE
IF(MM.NE.0) GO TO 613
IF(NN.LT.NEND) GO TO 10
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LE,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
8 FORMAT(1H0,32HNO. OF RECORDS IN MAGNETIC TAPE=I3)
GO TO 1111

1112 WRITE(6,38) IP,MAR
1111 STOP
END
SUBROUTINE RESID
RETURN
END
SUBROUTINE HAJIME
RETURN
END
SUBROUTINE RESID
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1H(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DO 1 K=1,3
DO 8 J=1,IMP1
DO 9 I=1,IMP1
E(I,J)=0.0
9 CONTINUE
CONTINUE
S=0.0
I1=LX1(K)
I2=LX2(K)
J1=LY1(K)
J2=LY2(K)
MIN=IND(K)
MININ=INDIN(K)
NUM=0
IF(K.EQ.1) J1=2
DO 3 J=J1,J2

```

```

JM1=J-1
JP1=J+1
CS=Y/X(J)
C1=X(JM1)/Y
SS=X(JP1)/Y
CB=-2.0*(CS+1.0/CS)
DO 4 I=I1,I2
MP=MPP(I,J)
MMM=(MP-MIN)* (MP-MININ)
IF(MMM.NE.0) GO TO 4
IP1=I+1
IM1=I-1
NUM=NUM+1
E(I,J)=E(I,J)+CB
E(IP1,J)=E(IP1,J)+CS
E(IM1,J)=E(IM1,J)+CS
E(I,JP1)=E(I,JP1)+SS
E(I,JM1)=E(I,JM1)+C1
4 CONTINUE
3 CONTINUE
IF(K.GE.2) GO TO 10
J1=3
DO 11 J=3,3
CS=Y/X(J)
E(3,J)=E(3,J)+CS
E(IM,J)=E(IM,J)+CS
11 CONTINUE
10 CONTINUE
DO 5 J=J1,J2
DO 6 I=I1,I2
IF(MPP(I,J).EQ.MIN) S=S+E(I,J)
6 CONTINUE
5 CONTINUE
NRES(K)=NUM
RES(K)=S
WRITE(6,7) K,NUM,S
7 FORMAT(1H ,2HK=I2,2X,12HGRID POINTS=I3,2X,4HRES=E15.7)
1 CONTINUE
DO 16 J=1,18
DO 17 I=1,IMP1
IF(MQQ(I,J).EQ.1) GO TO 17
MP=MPP(I,J)
IF(MP.EQ.2) GO TO 17
IF(MP.EQ.((MP/3)*3)) GO TO 18
IF(MP.EQ.((MP/4)*4)) GO TO 19
MQQ(I,J)=5
GO TO 17
18 MQQ(I,J)=3
GO TO 17
19 MQQ(I,J)=4
17 CONTINUE
16 CONTINUE
WRITE(6,15) (I,I=1,38)
15 FORMAT(1H ,4X,38I3)
DO 12 I=1,IMP1
WRITE(6,14) I,(MPP(I,J),J=1,38)
WRITE(6,13) I,(MQQ(I,J),J=1,38)
12 CONTINUE
13 FORMAT(1H ,I3,3X,38I3)
14 FORMAT(1H ,I3,2X,38I3)
RETURN
END
SUBROUTINE HAJIME

```

DATA:

IM, JM, IMH, JMH

OCEAN SHAPE (SUBROUTINE SHAPE 1)
 X,DX,DY (DX AND DY ARE THE GRID SIZES IN LONGITUDE AND
 LATITUDE (DEGREES), RESPECTIVELY. Y IS THE LATITUDE
 CORRESPONDING TO J=0).

AH,H,REL,DT,MAT

IT: IT=1 WIND STRESS IS READ TO COMPUTE THE WIND STRESS CURL.
 IT=2 WIND STRESS CURL IS GIVEN FROM CARDS, A MAGNETIC
 TAPE, OR THE SUBROUTINE CURL.

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
 1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
 2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
 3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
 4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
 5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
 DIMENSION L1(9),WE(147,39),WN(147,39),C(39)
 EQUIVALENCE (U(1),WE(1)),(V(1),WN(1))
 READ(5,40) IM,JM,IMH,JMH

40 FORMAT(4I5)

IMP1=IM+1

IMM1=IM-1

JMP1=JM+1

CALL SHAPE1

CALL SHAPE 1

DO 548 J=1,MM

DO 549 I=1,IMP1

F(I,J)=0.0

G(I,J)=0.0

U(I,J)=0.0

V(I,J)=0.0

XU(I,J)=0.0

XV(I,J)=0.0

549 CONTINUE

548 CONTINUE

READ(5,18) Y,DX,DY

18 FORMAT(3F10.0)

P=3.1415926/180.0

DX=DX*P

MM=JM+2

DO 100 I=1,MM

AR=(Y+DY*FLOAT(I))*P

F1=COS(AR)

X(I)=DX*F1

C(I)=F1

BET(I)=F1*X(I)*14.58E-5

100 CONTINUE

Y=DY*P

CD=14.58/(DX*Y)

DO 9997 J=1,JMP1

XM(J)=(X(J)+X(J+1))/2.0

FJU(J)=CD*(X(J)-X(J+1))

9997 CONTINUE

READ(5,16) AH,H,REL,DT,MAT

16 FORMAT(4E15.7,I5)

WRITE(6,17) AH,H,REL

17 FORMAT(1H,15HEDDY VISCOSITY=E15.7,10X,6HDEPTH=E15.7,10X,

115HRELAX ACCURACY=E15.7)

READ(5,10) IT

10 FORMAT(I5)

GO TO (1,2), IT

1 CONTINUE

CALL WIND

CALL WIND

P=0.01/4.0E5

DO 540 J=JMH,JMP1

XM1=XM(J)

```

JM1=J-1
XM1=XM(JM1)
DO 541 I=IMH, IM
IM1=I-1
TW(I,J)=(XMJ*(-WE(I,J)-WE(IM1,J))+XM1*(WE(I,JM1)+WE(IM1,JM1)))
1 + Y*(WN(I,J)+WN(I,JM1)-WN(IM1,J)-WN(IM1,JM1)))*P
41 CONTINUE
TW(1,J)=TW(IMM1,J)
TW(2,J)=TW(IM,J)
TW(IMP1,J)=TW(IMH,J)
540 CONTINUE
GO TO 3
2 CONTINUE
C CALL CURL
CALL CURL
READ(5,6004) (TW(I,J), I=3, IM)
6004 FORMAT(5E15.7)
TW(IMP1,J)=TW(3,J)
TW(2,J)=TW(IM,J)
TW(1,J)=TW(IMM1,J)
3 CONTINUE
C INITIAL GUESS
DO 4000 J=4, JM
CJ=1.0/(C(J)*Y*14.58E-5)/4.0
LJ=L(J)
DO 360 LL=1, LJ
II=KA(LL,J)
IG=KB(LL,J)
MP=II+IG
362 DO 361 I=II, IG
MM=MP-I
K=MM+1
P=F(K,J)-(TW(MM,J)+TW(K,J))*CJ
P(MM,J)=P
361 CONTINUE
IF(II.NE.3) GO TO 360
F(IMP1,J)=F(3,J)
360 CONTINUE
F(1,J)=F(IMM1,J)
F(2,J)=F(IM,J)
4000 CONTINUE
C INITIAL GUESS
CCC=2.0*Y
DO 4049 J=3, JM
JP1=J+1
LJ=LV(J)
DO 4058 LL=1, LJ
II=LA(LL,J)
IG=LB(LL,J)
DO 4053 I=II, IG
IP1=I+1
P=(F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCC
U(I,J)=P
XU(I,J)=P
P=(F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ
V(I,J)=P
XV(I,J)=P
53 CONTINUE
4058 CONTINUE
XU(IMP1,J)=XU(3,J)
XV(IMP1,J)=XV(3,J)
XU(2,J)=XU(IM,J)
XV(2,J)=XV(IM,J)
XU(1,J)=XU(IMM1,J)
XV(1,J)=XV(IMM1,J)
U(IMP1,J)=U(3,J)

```

V(1MP1,J)=V(3,J)
 U(2,J)=U(IM,J)
 V(2,J)=V(IM,J)
 U(1,J)=U(IMM1,J)
 V(1,J)=V(IMM1,J)

4049 CONTINUE

AR=AH/6.37E8/6.37E8

ARY=AR/Y

CCY=2.0*Y

Y4=Y*0.25

RETURN

END

SUBROUTINE SHAPE1

SUBROUTINE TO BE USED FOR THE BAROTROPIC PART OF THE WORLD OCEAN CIRCULATION WHEN THE SHAPE OF THE OCEAN IS CHANGED.

DATA: LV, LA AND LB FOR MQQ.

MM, M1(K), M2(K) AND M3(K) FOR MPP.

LV, LA AND LB ARE THE SAME AS THOSE USED FOR THE SUBROUTINE SHAPE 2 (BAROCLINIC PART), BUT THE DATA FOR MPP ARE DIFFERENT FROM THOSE USED FOR THE SHAPE2.

LX1, LX2, LY1, LY2 WHICH SPECIFY THE AREAS INCLUDING THE SEPARATE ISLANDS.

COMMON AH, DT, Y, H, REL, XM(39), FJU(39), X(39), F(147,39), E(147,39),
 1U(147,39), V(147,39), G(147,39), XU(147,39), XV(147,39), TW(147,39), CD,
 2BET(39), Y4, CCY, AR, ARY, RES(3), DDT,
 3MAT, L(39), LV(39), LA(10,37), LB(10,37), KA(10,37), KB(10,37), MATS,
 4MPP(147,39), MQQ(147,39), INDIN(3), IND(3), NRES(3),
 5LX1(3), LX2(3), LY1(3), LY2(3), IM, JM, IMP1, JMP1, IMM1

IMM1=IM-1

IMP1=IM+1

JMM1=JM-1

JMP1=JM+1

JMH=3

IMH=3

DO 30 J=1, JM

DO 31 I=1, IMP1

MQQ(I,J)=2

31 CONTINUE

30 CONTINUE

DO 32 J=3, JMM1

READ(5,33) M

33 FORMAT(I2)

READ(5,34) (LA(I,J), LB(I,J), I=1, M)

34 FORMAT(7(2I4, 2X))

DO 35 I=1, M

II=LA(I,J)

IG=LB(I,J)

DO 36 N=II, IG

MQQ(N,J)=1

36 CONTINUE

35 CONTINUE

LV(J)=M

MQQ(1,J)=MQQ(IMM1,J)

MQQ(2,J)=MQQ(IM,J)

MQQ(IMP1,J)=MQQ(3,J)

32 CONTINUE

DO 3006 J=3, 38

READ(5,3007) MM

3007 FORMAT(I2)

READ(5,3008) (M1(K), M2(K), M3(K), K=1, MM)

3008 FORMAT(8(2I4, I2))

DO 3009 K=1, MM

K5=M1(K)

K6=M2(K)

K7=M3(K)

DO 3010 I=K5, K6

```

MPP1(I,J)=K7
3010 CONTINUE
3009 CONTINUE
3006 CONTINUE
DO 3011 J=3,38
READ(5,3007) MM
L1(J)=MM
READ(5,3012) (KA1(LL,J),KB1(LL,J),LL=1,MM)
3012 FORMAT(16I5)
3011 CONTINUE
DO 6003 J=1,IMP1
MPP1(1,J)=MPP1(IMM1,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(IMP1,J)=MPP1(3,J)
6003 CONTINUE
DO 6004 J=3,JM
JP1=J+1
JM1=J-1
DO 6005 I=3,IM
IF(MPP1(I,J).GT.1) GO TO 6005
IF(MPP1(I-1,J).EQ.2) GO TO 6005
IF(MPP1(I,JP1).EQ.2) GO TO 6005
IF(MPP1(I,JM1).EQ.2) GO TO 6005
IF(MPP1(I+1,J).EQ.2) GO TO 6005
MPP1(I,J)=0
6005 CONTINUE
MPP1(IMP1,J)=MPP1(3,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(1,J)=MPP1(IMM1,J)
6004 CONTINUE
WRITE(6,6016) (J,J=3,38)
6016 FORMAT(1H ,5X,38I3/)
DO 6012 I=1,IMP1
WRITE(6,6014) I,(MPP1(I,J),J=3,38)
WRITE(6,6015) (MQQ(I,J),J=3,38)
6012 CONTINUE
6014 FORMAT(1H ,I3,2X,38I3)
6015 FORMAT(1H ,6X,38I3)
READ(5,2) (LX1(K),LX2(K),LY1(K),LY2(K),K=1,3)
2 FORMAT(4I5)
RETURN
END
SUBROUTINE WIND
COMMON AH,DT,Y,H,REL,XM(39),FJO(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DIMENSION WE(147,7),WN(147,7)
RETURN
END
SUBROUTINE CURL
RETURN
END

```

BAROTROPIC CIRCULATION IN A MULTI-CONNECTED GLOBAL OCEAN

MPP=0 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER POINTS,
 =1 IF ONE OF THE FOUR NEAREST SURROUNDING POINTS IS ON THE
 COAST OF THE MAIN LANDMASS (AFRICA, EUROPE, ASIA),
 =3 INSIDE THE ANTARCTICA,
 =30 ON THE COAST OF THE ANTARCTICA,
 =4 INSIDE AUSTRALIA,
 =40 ON THE COAST OF AUSTRALIA,
 =5 INSIDE NEWZEALAND,
 =50 ON THE COAST OF NEWZEALAND.

MULTIPLY THE STREAM FUNCTION VALUES BY R*H (R=EARTH'S
 RADIUS, H=OCEAN DEPTH) TO GET THE STREAM FUNCTION VALUES
 FOR THE VOLUME TRANSPORT (INTEGRAL OF THE HORIZONTAL VELOCITY
 OVER THE WHOLE DEPTH).

MQQ=1 FOR THE WATER POINTS,
 =2 FOR THE MAIN LAND MASS,
 =3 FOR THE ANTARCTICA,
 =4 FOR AUSTRALIA,
 =5 FOR NEWZEALAND.

THE SUBROUTINE HAJIME SPECIFY THE SHAPE OF THE OCEAN (MPP AND
 MQQ), THE WIND STRESS TO COMPUTE ITS CURL AND OTHER CONSTANTS
 AS WELL AS THE INITIAL FIELD OF THE STREAM FUNCTION.

THE SUBROUTINE RESID GIVES THE CHANGE OF THE SUM OF THE
 RESIDUALS (RES) AT EACH SEPARATE LAND MASS WHICH TAKES PLACE
 BY THE UNIT INCREASE OF THE STREAM FUNCTION AT EACH SEPARATE
 LAND MASS POINT, JUST AS IN CASE OF THE BLOCK RELAXATION.

F AND G DENOTE THE STREAM FUNCTION AT TIME STEP N+1, N,
 RESPECTIVELY, XU,XV,U, AND V THE BAROTROPIC COMPONENTS AT TIME
 STEPS N+1, N, RESPECTIVELY.

WIND STRESS CURL=-TW/(2.0*Y*X(J))/R*H

X, XM, Y=GRID SIZE

AH=COEFFICIENT OF EDDY VISCOSITY

DT IS THE TIME STEP.

H IS THE OCEAN DEPTH. CD IS THE TIME (DAY).

E IS THE WORKING SPACE FOR RELAXATION.

IM DENOTES THE EASTERNMOST POINTS TO BE SWEPT. (EX. 146)

JM DENOTES THE NORTHERNMOST PONTS TO BE SWEPT.

THE BACKWARD DIFFERENCING SCHEME IN TIME APPLIES EVERY MAT
 TIME STEPS. MATS CONTROLS THE SWITCHING FROM THE LEAP-FROG TO
 BACKWARD OF FROM THE BACKWARD TO LEAP-FROG SCHEMES.

PRINTING IS DONE EVERY NPRINT TIME STEPS.

WRINTING IN MAGNETIC TAPE IS DONE EVERY NTAPE TIME STEPS.

WHEN (IN) EQUALS ONE, THE IMAG-TH RECORD IN THE MAGNETIC TAPE
 IS PICKED UP, AND THE INTEGRATION GOES ON UNTIL NN=NEND.

REL=RELAXATION ACCURACY

WIND STRESS CURL=-TW(I,J)*H (DEPTH)/(2.0*Y*X(J)*RAD) RAD=

RADIUS OF THE EARTH)

IND(1)=30 ANTARCTIC COAST

IND(2)=40 AUSTRALIA COAST

IND(3)=50 NEWZEALAND COAST

INDIN(1)=3 ANTARCTIC INLAND

INDIN(2)=4 AUSTRALIA INLAND

INDIN(3)=5 NEWZEALAND INLAND

FIGURE 1 EXPLAINS THE MEANING OF LX1,LX2, LY1 AND LY2.

X=LX1	***	X=LX2
Y=LY2	***	Y=LY2

X=LX2
Y=LY2

X=LX1 ** X=LX2
Y=LY1 ** Y=LY1

FIG. 1

L, KA, KB SPECIFY THE STREAM FUNCTION POINTS TO BE SWEPT AND OTHER LAND POINTS TO BE SKIPPED.

FIGURE 2 EXPLAINS THEIR MEANINGS.

* POINT TO BE SWEPT

J=4 KA(1,J)***KB(1,J) KA(2,J)*****KB(2,J) KA(3,J)****KB(3,J)
L(J)=3

FIG. 2

THE COMPUTATION STOPS IF THE ENERGY EXCEEDS A CERTAIN VALUE, OR IF THE NUMBER OF ITERATION IN RELAXATION EXCEEDS A CERTAIN VALUE. THESE VALUES ARE SPECIFIED IN THE PROGRAM. THEY SHOULD BE CHANGED IF NECESSARY.

THE COEFFICIENT OF THE OVER-RELAXATION IS GIVEN AT THE BEGINNING.

```
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
SOR=1.775
SOR=1.875
SOR=1.825
SOR=1.85
SOR1=SOR-1.0
READ(5,1000) IN
1000 FORMAT(I5)
IF(IN.EQ.1) GO TO 1001
CALL HAJIME
CALL RESID
CD=0.0
NN=0
MAG=0
GO TO 5555
1001 CONTINUE
READ(5,1000) IMAG
IF(IMAG.EQ.1) GO TO 77
DO 7 J=2,IMAG
READ(10)
7 CONTINUE
77 READ(10) XU,XV,F,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
5555 CONTINUE
AH=1.0E9
AH=3.0E8
AR=AH/6.37E8/6.37E8
ARY=AR/Y
IMAG=NN+1
```

```

CNN=0.0
READ(5,5) NEND,MAT,NPRINT,NTAPE,DT,REL
5 FORMAT(4I5,2E15.7)
WRITE(6,6) IMAG,NEND,DT,REL,AH,MAT,NTAPE,NPRINT
6 FORMAT(1H ,16H TIME STEP FROM I5,2X,3HTO I5,2X,3HDT=E15.7,2X,4HREL
1=E15.7,2X,3HAH=E15.7,2X,4HMAT=I3/1H ,5HTAPE=I4,5X,6HPRINT=I4)
20 DAY=DT/0.864E5
MQQ(49,5)=1
MQQ(50,5)=1
MQQ(49,3)=3
MQQ(50,3)=3
39 NN=NN+1
CD=CD+DAY
NNN=(NN/MAT)*MAT
IF(NNN.EQ.NN) GO TO 25
MATS=0
DDT=DT
DO 1 J=3,JM
DO 2 I=1,IMP1
R=G(I,J)
G(I,J)=F(I,J)
F(I,J)=R
2 CONTINUE
1 CONTINUE
GO TO 26
25 MATS=1
DDT=DT*0.5
DO 42 J=3,JM
DO 43 I=1,IMP1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
G(I,J)=F(I,J)
43 CONTINUE
42 CONTINUE
26 CONTINUE
DO 30 J=3,JM
JP1=J+1
JM1=J-1
JM2=J-2
XMJ=XM(J)
XM1=XM(JM1)
C1=Y/XMJ
S1=Y/XM1
CB=X(JP1)/Y
CS=X(J)/Y
B=X(JM1)/Y
BETJ=BET(J)*CCY
LJ=L(J)
DO 31 LL=1,LJ
II=KA(LL,J)
MM=KB(LL,J)
DO 310 I=II,MM
IP1=I+1
IM1=I-1
IM2=I-2
UIJ=U(I,J)
VIJ=V(I,J)
UP1J=U(IP1,J)
UM1J=U(IM1,J)
UIP1=U(I,JP1)
UM1P1=U(IM1,JP1)
UIM1=U(I,JM1)
UM1M1=U(IM1,JM1)
UP1M1=U(IP1,JM1)
UIM2=U(I,JM2)
VIM2=V(I,JM2)

```

UM2J=U(IM2,J)
 VM2J=V(IM2,J)
 UM1M2=U(IM1,JM2)
 VM1M2=V(IM1,JM2)
 UM2M1=U(IM2,JM1)
 VM2M1=V(IM2,JM1)
 VP1J=V(IP1,J)
 VM1J=V(IM1,J)
 VIP1=V(I,JP1)
 VIM1=V(I,JM1)
 VM1P1=V(IM1,JP1)
 VM1M1=V(IM1,JM1)
 VP1M1=V(IP1,JM1)
 MP=MPE(I,J)
 IF(MP.EQ.0) GO TO 304
 IF(MP.EQ.30) GO TO 304
 IF(MP.EQ.50) GO TO 304
 IF(MQQ(IP1,J).NE.2) GO TO 27
 UP1J=-UIJ
 VP1J=-VIJ
 27 IF(MQQ(I,JP1).NE.2) GO TO 271
 UIP1=-UIJ
 VIP1=-VIJ
 271 IF(MQQ(IM1,JP1).NE.2) GO TO 272
 UM1P1=-UM1J
 VM1P1=-VM1J
 272 IF(MQQ(IM2,J).NE.2) GO TO 28
 UM2J=-UM1J
 VM2J=-VM1J
 28 IF(MQQ(IM2,JM1).NE.2) GO TO 29
 UM2M1=-UM1M1
 VM2M1=-VM1M1
 29 IF(MQQ(IM1,JM2).NE.2) GO TO 291
 UM1M2=-UM1M1
 VM1M2=-VM1M1
 291 IF(MQQ(I,JM2).NE.2) GO TO 292
 UIM2=-UIM1
 VIM2=-VIM1
 292 IF(MQQ(IP1,JM1).NE.2) GO TO 303
 UP1M1=-UIM1
 VP1M1=-VIM1
 303 CONTINUE
 304 DF=-BET J * (XV(I,J)+XV(IM1,J)+XV(IM1,JM1)+XV(I,JM1)) * 0.25
 SS=(C1*(UM1J+UIJ-UM2J-UP1J)-(UIP1-UIJ+UM1P1-UM1J)*CB+2.0*CS*
 1(UIJ-UIM1+UM1J-UM1M1)+S1*(UP1M1+UM2M1-UIM1-UM1M1)-(UIM1-UIM2+UM1M1
 2-UM1M2)*B)*ARY+TW(I,J)+DF
 DF=CS*(VIJ-VIM1-VM1J+VM1M1)
 SS=AR/XMJ*(C1*(-3.0*(VIJ-VM1J)+VP1J-VM2J)-DF
 1+(VIP1-VIJ-VM1P1+VM1J)*CB)+AR/XM1*(S1*(3.0*(VM1M1-VIM1)+VP1M1
 2-VM2M1)+(VM1M1-VM1M2-VIM1+VIM2)*B+DF)+SS
 4 E(I,J)=-SS*DDT
 310 CONTINUE
 31 CONTINUE
 E(2,J)=E(IM,J)
 E(IP1,J)=E(3,J)
 30 CONTINUE
 IP=0
 37 IP=IP+1
 C ***ISLANDS
 MAR=0
 C *****ANTARCTICA
 C *****NEWZEALAND
 C *****AUSTRALIA
 DO 5021 K=1,3
 RESK=RES(K)
 MP=IND(K)

```

      II=LX1(K)
      IG=LX2(K)
      IM2=LY1(K)
      JM2=LY2(K)
      R=0.0
      DO 5016 J=IM2,JM2
      DO 5015 I=II,IG
      IF(MPP(I,J).NE.MP) GO TO 5015
      R=R+E(I,J)
5015 CONTINUE
5016 CONTINUE
      IF(ABS(R).LE.REL) GO TO 5021
      DF=-R/RESK
      MAR=MAR+1
      IF(K.EQ.1) IM2=2
      DO 5022 J=IM2,JM2
      JP1=J+1
      JM1=J-1
      CS=Y/X(J)
      CB=2.0*(CS+1.0/CS)
      SS=X(JP1)/Y
      C1=X(JM1)/Y
      DO 5023 I=II,IG
      MPPIJ=MPP(I,J)
      MMMM=(MPPIJ-MP)*(MPPIJ-MPMP)
      IF(MMMM.NE.0) GO TO 5023
      F(I,J)=F(I,J)+DF
      IM1=I-1
      IP1=I+1
      CCC=DF*CS
      E(I,JP1)=E(I,JP1)+SS*DF
      E(I,JM1)=E(I,JM1)+C1*DF
      E(IP1,J)=E(IP1,J)+CCC
      E(IM1,J)=E(IM1,J)+CCC
      E(I,J)=E(I,J)-CB*DF
5023 CONTINUE
5022 CONTINUE
      IF(K.EQ.2) GO TO 5021
      IF(K.EQ.1) GO TO 5024
      DO 5026 J=8,12
      E(2,J)=E(IM,J)
5026 CONTINUE
      GO TO 5021
5024 CONTINUE
      E(IMP1,5)=E(3,5)
      E(2,5)=E(IM,5)
      CCC=DF*Y/X(4)
      E(3,4)=E(3,4)+CCC
      E(IM,4)=E(IM,4)+CCC
      E(IMP1,4)=E(3,4)
      E(2,4)=E(IM,4)
5021 CONTINUE
C*****NEWZEALAND
C*****ANTARCTICA
      DO 32 J=4,JM
      JM1=J-1
      JP1=J+1
      XJ=X(J)
      CS=Y/XJ
      SS=X(JP1)/Y
      C1=X(JM1)/Y
      CB=2.0*(CS+XJ/Y)
      LJ=L(J)
      DO 33 LL=1,LJ
      II=KA(LL,J)

```

```

MM=18(LL,J)
DO 330 I=II,MM
IF(MPP(I,J).GE.3) GO TO 330
R=E(I,J)
IF(ABS(R).LE.REL) GO TO 330
MAR=MAR+1
DF=R/CB*SOR
E(I,J)=-R*SOR1
F(I,J)=F(I,J)+DF
IP1=I+1
CCC=DF*CS
E(IP1,J)=E(IP1,J)+CCC
IM1=I-1
E(IM1,J)=E(IM1,J)+CCC
E(I,JP1)=E(I,JP1)+SS*DF
E(I,JM1)=E(I,JM1)+C1*DF
IF(I.NE.3) GO TO 331
E(IMP1,JP1)=E(3,JP1)
E(IMP1,JM1)=E(3,JM1)
E(IMP1,J)=E(3,J)
E(IM,J)=E(2,J)
GO TO 330
331 IF(I.NE.IM) GO TO 332
E(2,J)=E(IM,J)
E(2,JP1)=E(IM,JP1)
E(2,JM1)=E(IM,JM1)
E(3,J)=E(IMP1,J)
GO TO 330
332 IF(I.NE.4) GO TO 333
E(IMP1,J)=E(3,J)
GO TO 330
333 IF(I.NE.IMM1) GO TO 330
E(2,J)=E(IM,J)
330 CONTINUE
33 CONTINUE
32 CONTINUE
IF(MAR.EQ.0) GO TO 36
IF(IP.GT.1000) GO TO 1112
IF(IP.NE.1) GO TO 37
WRITE(6,38) IP,MAR
38 FORMAT(1H ,7X,6HKAISU=I5,5X,12HTEN NO. KAZU=I5)
GO TO 37
36 EN=0.0
WRITE(6,38) IP,MAR
DO 70 J=3,JM
F(1,J)=F(IMM1,J)
F(2,J)=F(IM,J)
F(IMP1,J)=F(3,J)
70 CONTINUE
DO 23 J=3,JM
JM1=J-1
JP1=J+1
XMJ=XM(J)*2.0
DF=XMJ*Y4
LVJ=LV(J)
DO 24 LJ=1,LVJ
II=LA(LJ,J)
IG=LB(LJ,J)
DO 244 I=II,IG
IP1=I+1
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
XU(I,J)=
1      (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
XV(I,J)=
1      (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ

```

30

```

EN=LN+DLM (AU(1,J)+Z+AV(1,J)+Z)
244 CONTINUE
24 CONTINUE
XU(IMP1,J)=XU(3,J)
XV(IMP1,J)=XV(3,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)
XU(2,J)=XU(IM,J)
XV(2,J)=XV(IM,J)
XU(1,J)=XU(IMM1,J)
XV(1,J)=XV(IMM1,J)
U(2,J)=U(IM,J)
V(2,J)=V(IM,J)
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
23 CONTINUE
WRITE(6,34) NN,CD,EN,F(1,3)
34 FORMAT(1H ,5HSTEP=I5,5X,5HTIME=E15.7,5X,7HENERGY=E15.7,5X,4HACC=F7
1.4)
IF(EN.GT.5.0E1) GO TO 1111
IF(NN.GE.NEND) GO TO 88
IF(MATS.NE.0) GO TO 10
IF(NN.EQ.((NN/NTAPE)*NTAPE)) GO TO 9
MAG=MAG+1
WRITE(10) XU,XV,F,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
9 IF(NN.EQ.((NN/NPRINT)*NPRINT)) GO TO 88
10 ENN=EN
IF(MATS.EQ.0) GO TO 39
MATS=MATS+1
IF(MATS.EQ.3) GO TO 46
DO 44 J=3,JM
DO 45 I=1,IMP1
F(I,J)=G(I,J)
U(I,J)=XU(I,J)
V(I,J)=XV(I,J)
45 CONTINUE
44 CONTINUE
GO TO 26
46 DO 47 J=3,JM
DO 48 I=1,IMP1
R=F(I,J)
F(I,J)=G(I,J)
G(I,J)=R
48 CONTINUE
47 CONTINUE
DO 49 J=3,JM
JP1=J+1
XMJ=XM(J)*2.0
LVJ=LV(J)
DO 55 LJ=1,LVJ
II=LA(LJ,J)
IG=LB(LJ,J)
DO 550 I=II,IG
IP1=I+1
U(I,J)=
1      (F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCY
V(I,J)=
1      (F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ
550 CONTINUE
55 CONTINUE
U(1,J)=U(IMM1,J)
V(1,J)=V(IMM1,J)
U(2,J)=U(IM,J)

```

```

V(2,J)=V(1,J)
U(IMP1,J)=U(3,J)
V(IMP1,J)=V(3,J)

49 CONTINUE
MATS=0
NN=NN+1
DDT=DT
NNT=NNT+1
CE=CD+DAY
GO TO 39

88 K=1
MP=-1
613 MP=MP+1
MM=K-MP
IG=18*MP+3
IF(MM.EQ.0) GO TO 614
II=IG+17
GO TO 615
614 II=38
615 WRITE(6,701)
701 FORMAT(1H0,15HSTREAM FUNCTION)
DO 702 J=1,IMP1
WRITE(6,703) J,(F(J,I),I=IG,II)
703 FORMAT(1H ,I3,1X,18F7.4)
702 CONTINUE
IF(MM.NE.0) GO TO 613
IF(NN.LT.NEND) GO TO 10
MAG=MAG+1
WRITE(10) XU,XV,P,G,U,V,TW,MPP,MQQ,L,KA,KB,LV,LA,LB,AH,DT,MAT,
1Y,REL,XM,FJU,X,BET,LX1,LX2,LY1,LY2,IND,INDIN,NN,NEND,RES,
2NRES,ARY,AR,Y4,E,CCY,MATS,CD,IM,JM,IMP1,JMP1,IMM1,MAG
WRITE(6,8) MAG
8 FORMAT(1H0,32HNO. OF RECORDS IN MAGNETIC TAPE=I3)
GO TO 1111
1112 WRITE(6,38) IP,MAR
1111 STOP
END
SUBROUTINE RESID
RETURN
END
SUBROUTINE HAJIME
RETURN
END
SUBROUTINE RESID
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KE(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DO 1 K=1,3
DO 8 J=1,IMP1
DO 9 I=1,IMP1
E(I,J)=0.0
9 CONTINUE
8 CONTINUE
S=0.0
I1=LX1(K)
I2=LX2(K)
J1=LY1(K)
J2=LY2(K)
MIN=IND(K)
MININ=INDIN(K)
NUM=0
IF(K.EQ.1) J1=2
DO 3 J=J1,J2

```

```

JM1=J-1
JP1=J+1
CS=Y/X(J)
C1=X(JM1)/Y
SS=X(JP1)/Y
CB=-2.0*(CS+1.0/CS)
DO 4 I=I1,I2
MP=MPP(I,J)
MMM=(MP-MIN)*(MF-MININ)
IF(MMM.NE.0) GO TO 4
IP1=I+1
IM1=I-1
NUM=NUM+1
E(I,J)=E(I,J)+CB
E(IP1,J)=E(IP1,J)+CS
E(IM1,J)=E(IM1,J)+CS
E(I,JP1)=E(I,JP1)+SS
E(I,JM1)=E(I,JM1)+C1
4 CONTINUE
3 CONTINUE
IF(K.GE.2) GO TO 10
J1=3
DO 11 J=3,3
CS=Y/X(J)
E(3,J)=E(3,J)+CS
E(IM,J)=E(IM,J)+CS
11 CONTINUE
10 CONTINUE
DO 5 J=J1,J2
DO 6 I=I1,I2
IF(MPP(I,J).EQ.MIN) S=S+E(I,J)
6 CONTINUE
5 CONTINUE
NRES(K)=NUM
RES(K)=S
WRITE(6,7) K,NUM,S
7 FORMAT(1H ,2HK=I2,2X,12HGRID POINTS=I3,2X,4HRES=E15.7)
1 CONTINUE
DO 16 J=1,18
DO 17 I=1,IMP1
IF(MQQ(I,J).EQ.1) GO TO 17
MP=MPP(I,J)
IF(MP.EQ.2) GO TO 17
IF(MP.EQ.((MP/3)*3)) GO TO 18
IF(MP.EQ.((MP/4)*4)) GO TO 19
MQQ(I,J)=5
GO TO 17
18 MQQ(I,J)=3
GO TO 17
19 MQQ(I,J)=4
17 CONTINUE
16 CONTINUE
WRITE(6,15) (I,I=1,38)
15 FORMAT(1H ,4X,38I3)
DO 12 I=1,IMP1
WRITE(6,14) I,(MPP(I,J),J=1,38)
WRITE(6,13) I,(MQQ(I,J),J=1,38)
12 CONTINUE
13 FORMAT(1H ,I3,3X,38I3)
14 FORMAT(1H ,I3,2X,38I3)
RETURN
END
SUBROUTINE HAJIME

```

C
C DATA:
C IM, JM, IMH, JMH

OCEAN SHAPE (SUBROUTINE SHAPE 1)
 X,DX,DY (DX AND DY ARE THE GRID SIZES IN LONGITUDE AND
 LATITUDE (DEGREES), RESPECTIVELY. Y IS THE LATITUDE
 CORRESPONDING TO J=0).

AH,H, REL,DT,MAT

IT: IT=1 WIND STRESS IS READ TO COMPUTE THE WIND STRESS CURL.
 IT=2 WIND STRESS CURL IS GIVEN FROM CARDS, A MAGNETIC
 TAPE, OR THE SUBROUTINE CURL.

COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),F(147,39),E(147,39),
 1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
 2BET(39),Y4,CCY,AR,ARY,RES(3),DDT,
 3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
 4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
 5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
 DIMENSION L1(9),WE(147,39),WN(147,39),C(39)
 EQUIVALENCE (U(1),WE(1)),(V(1),WN(1))
 READ(5,40) IM,JM,IMH,JMH

40 FORMAT(4I5)

IMP1=IM+1

IMM1=IM-1

JMP1=JM+1

CALL SHAPE1

CALL SHAPE 1

DO 548 J=1,MM

DO 549 I=1,IMP1

F(I,J)=0.0

G(I,J)=0.0

U(I,J)=0.0

V(I,J)=0.0

XU(I,J)=0.0

XV(I,J)=0.0

549 CONTINUE

548 CONTINUE

READ(5,18) Y,DX,DY

18 FORMAT(3F10.0)

P=3.1415926/180.0

DX=DX*P

MM=JM+2

DO 100 I=1,MM

AR=(Y+DY*FLOAT(I))*P

F1=CCS(AR)

X(I)=DX*F1

C(I)=F1

BET(I)=F1*X(I)*14.58E-5

100 CONTINUE

Y=DY*P

CD=14.58/(DX*Y)

DO 9997 J=1,JMP1

XM(J)=(X(J)+X(J+1))/2.0

FJU(J)=CD*(X(J)-X(J+1))

9997 CONTINUE

READ(5,16) AH,H,REL,DT,MAT

16 FORMAT(4E15.7,I5)

WRITE(6,17) AH,H,REL

17 FORMAT(1H,15HEDDY VISCOSITY=E15.7,10X,6HDEPTH=E15.7,10X,

115HRELAX ACCURACY=E15.7)

READ(5,10) IT

10 FORMAT(I5)

GO TO (1,2), IT

1 CONTINUE

CALL WIND

CALL WIND

P=0.01/4.0E5

DO 540 J=JMH,JMP1

XMJ=XM(J)

```

J=I-J-1
XM1=XM(JM1)
DO 541 I=IMH, IM
IM1=I-1
TW(I,J)=(XMJ*(-WE(I,J)-WE(IM1,J))+XM1*(WE(I,JM1)+WE(IM1,JM1)))
1 + Y*(WN(I,J)+WN(I,JM1)-WN(IM1,J)-WN(IM1,JM1)))*P
541 CONTINUE
TW(1,J)=TW(IMM1,J)
TW(2,J)=TW(IM,J)
TW(IMP1,J)=TW(IMH,J)
540 CONTINUE
GO TO 3
2 CONTINUE
C CALL CURL
CALL CURL
READ(5,6004) (TW(I,J),I=3,IM)
6004 FORMAT(5E15.7)
TW(IMP1,J)=TW(3,J)
TW(2,J)=TW(IM,J)
TW(1,J)=TW(IMM1,J)
3 CONTINUE
C INITIAL GUESS
DO 4000 J=4, JM
CJ=1.0/(C(J)*Y*14.58E-5)/4.0
LJ=L(J)
DO 360 LL=1,LJ
II=KA(LL,J)
IG=KB(LL,J)
MP=II+IG
362 DO 361 I=II,IG
MM=MP-I
K=MM+1
P=F(K,J)-(TW(MM,J)+TW(K,J))*CJ
F(MM,J)=P
361 CONTINUE
IF(II.NE.3) GO TO 360
F(IMP1,J)=F(3,J)
360 CONTINUE
F(1,J)=F(IMM1,J)
F(2,J)=F(IM,J)
4000 CONTINUE
C INITIAL GUESS
CCC=2.0*Y
DO 4049 J=3, JM
JP1=J+1
LJ=LV(J)
DO 4058 LL=1,LJ
II=LA(LL,J)
IG=LB(LL,J)
DO 4053 I=II,IG
IP1=I+1
P=(F(I,J)+F(IP1,J)-F(I,JP1)-F(IP1,JP1))/CCC
U(I,J)=P
XU(I,J)=P
P=(F(IP1,J)+F(IP1,JP1)-F(I,J)-F(I,JP1))/XMJ
V(I,J)=P
XV(I,J)=P
53 CONTINUE
58 CONTINUE
XU(IMP1,J)=XU(3,J)
XV(IMP1,J)=XV(3,J)
XU(2,J)=XU(IM,J)
XV(2,J)=XV(IM,J)
XU(1,J)=XU(IMM1,J)
XV(1,J)=XV(IMM1,J)
U(IMP1,J)=U(3,J)

```

V(IMP1,J)=V(3,J)
 U(2,J)=U(IM,J)
 V(2,J)=V(IM,J)
 U(1,J)=U(IMM1,J)
 V(1,J)=V(IMM1,J)

4049 CONTINUE
 AR=AH/6.37E8/6.37E8
 ARY=AR/Y
 CCY=2.0*Y
 Y4=Y*0.25
 RETURN
 END

SUBROUTINE SHAPE1

C SUBROUTINE TO BE USED FOR THE BAROTROPIC PART OF THE WORLD OCEAN
 C CIRCULATION WHEN THE SHAPE OF THE OCEAN IS CHANGED.

C DATA: LV, LA AND LB FOR MQQ.

C MM, M1(K), M2(K) AND M3(K) FOR MPP.

C LV, LA AND LB ARE THE SAME AS THOSE USED FOR THE SUBROUTINE
 C SHAPE 2 (BAROCLINIC PART), BUT THE DATA FOR MPP ARE DIFFERENT
 C FROM THOSE USED FOR THE SHAPE2.

C LX1, LX2, LY1, LY2 WHICH SPECIFY THE AREAS INCLUDING THE SEPARATE
 C ISLANDS.

COMMON AH, DT, Y, H, REL, XM(39), FJU(39), X(39), F(147,39), E(147,39),
 1U(147,39), V(147,39), G(147,39), XU(147,39), XV(147,39), TW(147,39), CD,
 2BET(39), Y4, CCY, AR, ARY, RES(3), DDT,
 3MAT, L(39), LV(39), LA(10,37), LB(10,37), KA(10,37), KB(10,37), MATS,
 4MPP(147,39), MQQ(147,39), INDIN(3), IND(3), NRES(3),
 5LX1(3), LX2(3), LY1(3), LY2(3), IM, JM, IMP1, JMP1, IMM1

IMM1=IM-1

IMP1=IM+1

JMM1=JM-1

JMP1=JM+1

JMH=3

IMH=3

DO 30 J=1, JM

DO 31 I=1, IMP1

MQQ(I,J)=2

31 CONTINUE

30 CONTINUE

DO 32 J=3, JMM1

READ(5,33) M

33 FORMAT(I2)

READ(5,34) (LA(I,J), LB(I,J), I=1, M)

34 FORMAT(7(2I4, 2X))

DO 35 I=1, M

II=LA(I,J)

IG=LB(I,J)

DO 36 N=II, IG

MQQ(N,J)=1

36 CONTINUE

35 CONTINUE

LV(J)=M

MQQ(1,J)=MQQ(IMM1,J)

MQQ(2,J)=MQQ(IM,J)

MQQ(IMP1,J)=MQQ(3,J)

32 CONTINUE

DO 3006 J=3, 38

READ(5,3007) MM

FORMAT(I2)

READ(5,3008) (M1(K), M2(K), M3(K), K=1, MM)

3008 FORMAT(8(2I4, I2))

DO 3009 K=1, MM

K5=M1(K)

K6=M2(K)

K7=M3(K)

DO 3010 I=K5, K6

3007

```

MPP1(I,J)=K7
3010 CONTINUE
3009 CONTINUE
3006 CONTINUE
DO 3011 J=3,38
READ(5,3007) MM
L1(J)=MM
READ(5,3012) (KA1(LL,J),KB1(LL,J),LL=1,MM)
3012 FORMAT(16I5)
3011 CONTINUE
DO 6003 J=1, JMP1
MPP1(1,J)=MPP1(IMM1,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(IMP1,J)=MPP1(3,J)
6003 CONTINUE
DO 6004 J=3,JM
JP1=J+1
JM1=J-1
DO 6005 I=3,IM
IF(MPP1(I,J).GT.1) GO TO 6005
IF(MPP1(I-1,J).EQ.2) GO TO 6005
IF(MPP1(I,JP1).EQ.2) GO TO 6005
IF(MPP1(I,JM1).EQ.2) GO TO 6005
IF(MPP1(I+1,J).EQ.2) GO TO 6005
MPP1(I,J)=0
6005 CONTINUE
MPP1(IMP1,J)=MPP1(3,J)
MPP1(2,J)=MPP1(IM,J)
MPP1(1,J)=MPP1(IMM1,J)
6004 CONTINUE
WRITE(6,6016) (J,J=3,38)
6016 FORMAT(1H ,5X,38I3/)
DO 6012 I=1,IMP1
WRITE(6,6014) I,(MPP1(I,J),J=3,38)
WRITE(6,6015) (MQQ(I,J),J=3,38)
6012 CONTINUE
6014 FORMAT(1H ,I3,2X,38I3)
6015 FORMAT(1H ,6X,38I3)
READ(5,2) (LX1(K),LX2(K),LY1(K),LY2(K),K=1,3)
2 FORMAT(4I5)
RETURN
END
SUBROUTINE WIND
COMMON AH,DT,Y,H,REL,XM(39),FJU(39),X(39),P(147,39),E(147,39),
1U(147,39),V(147,39),G(147,39),XU(147,39),XV(147,39),TW(147,39),CD,
2BET(39),Y4,CCY,AR,ARY,RES(3), DDT,
3MAT,L(39),LV(39),LA(10,37),LB(10,37),KA(10,37),KB(10,37),MATS,
4MPP(147,39),MQQ(147,39),INDIN(3),IND(3),NRES(3),
5LX1(3),LX2(3),LY1(3),LY2(3),IM,JM,IMP1,JMP1,IMM1
DIMENSION WE(147,7),WN(147,7)
RETURN
END
SUBROUTINE CURL
RETURN
END

```

MPP
 MPP=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,
 =2 ON THE LAND (EXCLUDING THE COAST LINE).
 FOR THE COAST-POINTS, REFER TO FIG.1.

14
 34XXXXXXXXXXXXXXX33
 XXXXXLANDXXXXX
 XXXXXXXXX
 XX22 21XX
 11XX XX13
 XX XX
 XX23 24XX
 XXXXXXXXX
 31XXXXXXXXXXXXX32
 12

FIG.1

MQQ

MQQ=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,
 =2 ON THE LAND.
 IN OTHER CASES, REFER TO FIG.2.

1112
 XXXXXXXX
 XXXXXLANDXXXXX
 XXXXXX
 XX1221 2211XX
 XX XX
 2111XX XX1121
 XX XX
 XX1122 2112XX
 XXXXXXXXX
 XXXXXXXX
 1211

FIG.2

COMMON T(147,39,5), TT(147,39,5), SP(147,39), AT(5), UU(147,39,5),
 IVV(147,39,5), U(147,39,5), V(147,39,5), W(147,39,5), UB(147,39),
 2VB(147,39), WE(147,39), WN(147,39), Q(39), YJA(38), XHT(38), XHS(38),
 3 XMY(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,
 4GAM, Y, YY, B, RR, HH, H2, AZHH, R2, AHY, AHRF, AH2, BB, BE2, AAA, BBB, DDT, A1, UV,
 5UUU, VVV, RRH, AQ, GAM2, AL2, BUN, BY, AM, AMRR, GAMGAM, AJAL, BAN, KMP1,
 6MPP(147,39), MQQ(147,39), IM, JM, KM, IMM1, JMM1, KMM1, TMP1, JMP1, MAT,
 7 NK, NNNN, IMH, JMH, MATS, L(39), KA(10,39), KB(10,39), LV(39), NEND,
 8LA(10,39), LB(10,39), NN, TE(147,46), UN(147,39), TD(147,46), RN(147,39)
*, CL(147,39)

DIMENSION UHEAD(39), THEAD(39)
 DIMENSION QE(147,39), QH(147,39), QSH(147,39)

COMMON /TEMP/ QE, QH, QSH, ZQE, ZQH, ZSH, ZRN

DIMENSION ZQE(39), ZQH(39)

LOGICAL STOP

REAL KK

DIMENSION ZRN(39), ZSH(39)

DIMENSION ZT(39,5), ZW(39,5), UZ(39,5), VZ(39,5)

EQUIVALENCE (TT(1), UZ(1)), (ZW(1), VZ(1)), (ZT(1), W(1)), (ZW(1), W(196))

DIMENSION ICTL(7), RCTL(2), FIELD(18)

DATA ICTL/1,6,9,1,18,7,2/

DATA RCTL /0.001,60./

```

      FORMATTED, 308, 'EXPERIMENTAL OR CALCULATED RADIAZATION')

UHEAD(1) = -72.
THEAD(1) = -74.
DO 88 I=2,39
UHEAD(I) = UHEAD(1) + 4.* (I-1)
THEAD(I) = THEAD(1) + 4.* (I-1)
CONTINUE

      NNNN=0
      READ(5,9) KT
      READ(5,9) IN
9 FORMAT(I5)
      IF(IN.EQ.0) GO TO 11
17   READ(KT,END=92)
*           TT, UU, VV, T, U, V, AT, SP, W, UB, VB, X, XM, Q, PU, FJU, DT, AZ, AH, WE,
1WN, BAN, AL, GAM, Y, YY, R, RR, HH, H2, AZHH, BUN, R2, AHY, AHRE, AH2, PB, BB2,
2AAA, BBB, DDT, A1, UV, UUU, VVV, RRH, AQ, GAM2, AL2, RY, ANRR, GAMGAM, ALAL,
3H, Z, ZZ, AM, XJA, XHT, XHS, XMY, CD,
4MPP, MQQ, KA, KB, L, LA, LB, LV, MATS, NEND, NK, NNNN, MAT, IM, JM, KM, IMH, IMM1,
5IMP1, KMP1, KMM1, JMM1, JMP1, MN, JMH, MAG, TE, TD, RN
6, QE, QH, QSH, CL, UN
      GO TO 17
92 BACK SPACE KT
      IF(MAG.LT.34) GO TO 94
      REWIND KT
      KT = KT + 1
      MAG=0
94   CONTINUE
73   READ(10,END=74) UR,VB
      GO TO 73
74   REWIND 10
      DO 2222 I=1,145
      WRITE(6,7000) I, (UN(I,J), J=3,20)
2222 CONTINUE
      DO 4444 I=1,145
      WRITE(6,7000) I, (UN(I,J), J=21,38)
4444 CONTINUE
      WRITE(6,890) (THEAD(J), J=3,20)
      DO 7040 I=1,147
      WRITE(6,7000) I, (TE(I,J), J=3,20)
7040 CONTINUE
      WRITE(6,890) (THEAD(J), J=21,38)
      DO 7034 I=1,147
      WRITE(6,7000) I, (TE(I,J), J=21,38)
7034 CONTINUE
      CL(1,3)=6.00
      CL(2,3)=6.00
      CL(145,3)=6.00
      CL(146,3) = 6.
      CL(147,3) = 6.
      DO 3333 I=1,145
      WRITE(6,7000) I, (CL(I,J), J=3,20)
3333 CONTINUE
      DO 5555 I=1,145
      WRITE(6,7000) I, (CL(I,J), J=21,38)
5555 CONTINUE
      FA=400000.
      DO 311 I=1,147
      WE(I,3)=1.16*FA
      WE(I,4)=1.72*FA
      WE(I,5)=1.83*FA
      WE(I,6)=1.90*FA
      WE(I,7)=1.83*FA
      WE(I,8)=1.50*FA
      WE(I,9)=1.10*FA
      WE(I,10)=0.72*FA

```

```

WE(I,11)=-0.50*FA
WE(I,12)=-0.07*FA
WE(I,13)=-0.30*FA
WE(I,14)=-0.52*FA
WE(I,15)=-0.60*FA
WE(I,16)=-0.60*FA
WE(I,17)=-0.52*FA
WE(I,18)=-0.38*FA
WE(I,19)=-0.30*FA
WE(I,20)=-0.24*FA
WE(I,21)=-0.26*FA
WE(I,22)=-0.38*FA
WE(I,23)=-0.50*FA
WE(I,24)=-0.53*FA
WE(I,25)=-0.40*FA
WE(I,26)=-0.14*FA
WE(I,27)=0.10*FA
WE(I,28)=0.42*FA
WE(I,29)=0.61*FA
WE(I,30)=0.74*FA
WE(I,31)=0.78*FA
WE(I,32)=0.63*FA
WE(I,33)=0.48*FA
WE(I,34)=0.14*FA
WE(I,35)=+0.01*FA
WE(I,36)=-0.04*FA
WE(I,37)=-0.13*FA
311 CONTINUE
AH=2.5E7
AHY=AH*Y
AHRP=AH/RR
AH2=AH/(YY*RR)
AL=0.25E-3
ALAL=AL*2.0
AL2=AL/2.0
AZ=1.0
AZHH=AZ/HH
GAMGAM=25.0*H/(AZ*0.864E5)
WRITE(6,7777)
WRITE(6,9005)
9005 FORMAT(1H0,21HBAROTROPIC COMPONENTS/)
WRITE(6,9110)
9110 FORMAT(1X,'UB')
WRITE(6,9004) (J,J=3,21)
9004 FORMAT(1H0,4X,19(2X,J2,2X)/)
DO 9000 I=1,147
WRITE(6,9001) I,(UB(I,J),J=3,21),I
9000 CONTINUE
WRITE(6,7777)
WRITE(6,9004) (J,J=20,38)
DO 9002 I=1,147
WRITE(6,9001) I,(UB(I,J),J=20,38),I
9002 CONTINUE
WRITE(6,7777)
WRITE(6,9200)
9200 FORMAT(1X,'VB')
WRITE(6,9004) (J,J=3,21)
DO 9006 I=1,147
WRITE(6,9001) I,(VB(I,J),J=3,21),J
9006 CONTINUE
WRITE(6,7777)
WRITE(6,9004) (J,J=20,38)
DO 9007 I=1,147
WRITE(6,9001) I,(VB(I,J),J=20,38),I
9007 CONTINUE
9001 FORMAT(1H ,I3,1X,19F6.2,1X,I3)

```

```

      WRITE(6,9100) (Q(J),J=3,33)
9100 FORMAT(1H0,18F6.2/1H ,18F6.2/)
      IF(NK.NE.3) GO TO 492
      GO TO 5
11 CONTINUE
      NN=0
      CD=0.0
      NK=3
      MAG=0
      CALL FREP
      CALL FRPFA
      CALL GEOST
      5 READ(5,3) MATS, NEND, NPRINT, NTAPE, DT
      3 FORMAT(4I5,E15.7)
      WRITE(6,6) NPRINT, NTAPE
      6 FORMAT(' NPRINT = ',I5,' NTAPE = ',I5)
      WRITE(6,8) KT, MAG, CD
      8 FORMAT(' KT = ',I2,' MAG = ',I2,' CD = ',F7.1)
      DTD=DT/0.864E5
      K=NN+1
      NEND=NEND+K
      WRITE(6,4) K, NEND, MATS, DT,AZ,AM,AH
      4 FORMAT(' ', 'TIME STEP FROM ',I5,3X,' TO ',I5,5X,'MATS=',I3,5X,
      X 'DT=',4E15.7/)
      IF(DT.LT.10.) STOP 100
      DDT=DT*2.0
      DO 111 J=JMH,JMM1
      XJ=FJU(J)*DDT
      XJA(J)=XJ*AAA
      XHT(J)=1.0/(1.0+XJA(J)**2)
      XHS(J)=XJ*BBB
      XMY(J)=Y*XM(J)
111 CONTINUE
      IF(NN.GT.0) GO TO 251
      CALL CONTI
      MAT=2
      WRITE(2) TT
      REWIND 2
      WRITE(3) U,V
      REWIND 3
      DDT=DT
      GO TO 253
-251 NN=NN+1
      CD=CD+DTD
      NNN=(NN/MATS)*MATS
      IF(NNN.NE.NN) GO TO 250
      MAT=1
      WRITE(6,2)
      2 FORMAT(1H ,5H BEGIN)
250 CONTINUE
253 CALL THERME
      CALL EQA
      CALL CONTI
      WRITE(6,7013) UUU,VVV,UV,MN,CD
7013 FORMAT(1H ,7H ENERGY=3(E15.7,3X),5HSTEP=I5,2X,4H DAY=F10.2)
      IF(MAT.NE.0) GO TO 7019
      CALL WTO(STOP)
      IF(STOP) NEND=10
      IF(NN.GE.NEND) GO TO 7015
      IF(((NN/NTAPE)*NTAPE).NE.NN) GO TO 7025
      IF(NN.EQ.0) GO TO 7019
7015 MAG = MAG+1
      WTM = 0.0
      GQSH = 0.0
      GQE=0.0
      GQH = 0.0

```

6 |

```

GRN = 0.
DO 2001 J=3,38
DXYP = X(J) * Y
CLAT = ABS(DXYP)
KK=0.
ZQH(J) = 0.
ZQE(J) = 0.0
ZZZ=0.
ZRN(J) = 0.
DO 2002 I=3,146
IF (MPP(I,J).GT.1.AND.MPP(I,J).LE.5) GO TO 9011
UM=UN(I,J)*51.48
TEIJ=TE(I,J)
TIJ= T(I,J,1)
TW=TD(I,J)+273.15
123 TS=T(I,J,1)+273.15
PCB=1013.25*0.1
ESS=10.0** (8.4051-2353.0/TS)
ESD=10.0** (8.4051-2353.0/TW)
QS=0.622*ESS/(PCB-ESS)
QA=0.622*ESD/(PCB-ESD)
IF (((TIJ-TEIJ)+0.609* TS*(QS-QA)).LT.0.0) GO TO 334
332 CU=0.033
CO=1.23*0.001
GO TO 133
334 CU=0.018
CO=0.41*0.001
133 QH(I,J)=-1.2*0.001*.24*CO*UM*(TIJ-TEIJ)*0.864E5
QE(I,J)=-1.2*0.001*CO*595.*UM*(QS-QA)*0.864E5
RN(I,J)=RN(I,J)*0.864E5
QSH(I,J)=RN(I,J)+QH(I,J)+QE(I,J)
GQSH = GQSH+QSH(I,J)*CLAT
GQE = GQE + QE(I,J)*CLAT
GQH = GQH + QH(I,J)*CLAT
GRN = GRN + RN(I,J) * CLAT
WTM = WTM+CLAT
KK=KK+1.
ZZZ = QSH(I,J) + ZZZ
ZQH(J) = QH(I,J) + ZQH(J)
ZQE(J) = QE(I,J) + ZQE(J)
ZRN(J) = RN(I,J) + ZRN(J)
GO TO 2002
9011 QSH(I,J) = 0.
QE(I,J) = 0.
QH(I,J) = 0.
2002 CONTINUE
KK = 1./KK
ZSH(J) = ZZZ*KK
ZQE(J) = ZQE(J) * KK
ZQH(J) = ZQH(J)*KK
ZRN(J) = ZRN(J) * KK
2001 CONTINUE
WTM = 1./WTM
GQSH = GQSH*WTM
GQE = GQE*WTM
GQH = GQH*WTM
GRN = GRN*WTM
WRITE(KT)
* TT, UU, VV, T, U, V, AT, SP, W, UB, VR, X, XM, Q, FU, FJU, DT, AZ, AH, RE,
1WN, BAN, AL, GAM, Y, YY, R, RP, HH, H2, AZHH, BUN, R2, AHY, AHFF, AH2, BB, BB2,
2AAA, BBB, DDT, A1, UV, UUU, VVV, RRH, AC, GAM2, AL2, RY, AMRP, GAMGAM, ALAL,
3H, Z, ZZ, AM, XJA, XHT, XHS, XMY, CD,
4MPP, MQQ, KA, KB, L, LA, LB, LV, MATS, NEND, NK, NNNN, MAT, IM, JM, KM, LMH, IMM1,
5IMP1, KMM1, JMM1, JMP1, NN, JMH, MAG, TE, TD, RN
*, QE, QH, QSH, CL, UN
ENDFILE KT

```

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BACKSPACE K1
WRITE(6,1) MAG
1 FORMAT(1H ,35HNUMBER OF RECORDS IN MAGNETIC TAPE=I2)
IF(NN.GE.NEND) GO TO 7014
IF(MAG.GT.34) GO TO 93
7025 IF(UV.GT.1.0E26) GO TO 7014
7014 IF(((NN/NPRINT)*NPRINT).NE.NN) GO TO 7019
7020 WRITE(6,7020) NN,CD
FORMAT(1H ,11HTIME(STEP)=I8.5X,10HTIME(DAY)=E15.7)
DO 300 K=1,5
KK=0.
DO 301 J=3,38
UZSUM=0.
VZSUM=0.
DO 303 I=3,146
IF(MQQ(I,J).LE.5.AND.MQQ(I,J).NE.1) GO TO 303
KK=KK+1.
UZSUM=UZSUM+U(I,J,K)
VZSUM=VZSUM+V(I,J,K)
303 CONTINUE
IF(KK.LT.1) GO TO 300
UZ(J,K)=UZSUM/KK
VZ(J,K)=VZSUM/KK
301 CONTINUE
300 CONTINUE
DO 7009 K=1,KM
WRITE(6,7777)
WRITE(6,7010) K, CD
7010 FORMAT(1X,'UU AT K = ',I1,', DAY ',F7.1)
WRITE(6,890) (UHEAD(J),J=3,20)
DO 7011 I=IMH,IM
WRITE(6,7012) I,(UU(I,J,K),J=3,20)
7012 FORMAT(1H ,I3,1X,18F7.2)
7011 CONTINUE
WRITE(6,7778) (UZ(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7010) K,CD
WRITE(6,890) (UHEAD(J),J=21,38)
DO 7022 I=IMH,IM
WRITE(6,7012) I,(UU(I,J,K),J=21,38)
7022 CONTINUE
WRITE(6,7778) (UZ(J,K),J=21,38)
7009 CONTINUE
DO 7070 K=1,KM
WRITE(6,7777)
WRITE(6,7053) K,CD
WRITE(6,890) (UHEAD(J),J=3,20)
7053 FORMAT(1X,'VV AT K = ',I1,', DAY ',F7.1)
DO 7021 I=IMH,IM
WRITE(6,7012) I,(VV(I,J,K),J=3,20)
7021 CONTINUE
WRITE(6,7778) (VZ(J,K),J=3,20)
890 FORMAT(/5X,18F7.2/)
WRITE(6,7777)
WRITE(6,7053) K,CD
WRITE(6,890) (UHEAD(J),J=21,38)
DO 7023 I=IMH,IM
WRITE(6,7012) I,(VV(I,J,K),J=21,38)
7023 CONTINUE
WRITE(6,7778) (VZ(J,K),J=21,38)
7070 CONTINUE
DO 200 K=1,KM
DO 201 J=3,38
KK=0.
WZSUM=0.
TZSUM=0.

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DO 203 I=3,146
IF(MPP(I,J).GT.1.AND. MPP(J,J).LE.5) GO TO 203
KK=KK+1.
WZSUM=WZSUM+W(I,J,K)
TZSUM=TZSUM+TT(I,J,K)
203 CONTINUE
IF(KK.LT.1) GO TO 200
ZW(J,K)=WZSUM/KK
ZT(J,K)=TZSUM/KK
201 CONTINUE
200 CONTINUE
DO 7005 K=1,KM
WRITE(6,7777)
WRITE(6,7006) K
7006 FORMAT(1H ,17 HTEMPERATURE AT K=I1)
WRITE(6,890) (THEAD(J),J=3,20)
DO 7050 I=IMH,IM
WRITE(6,7000) I,(TT(I,J,K),J=3,20)
7050 CONTINUE
WRITE(6,7778) (ZT(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7006) K
WRITE(6,890) (THEAD(J),J=21,38)
DO 7051 I=IMH,IM
WRITE(6,7000) I,(TT(I,J,K),J=21,38)
7051 CONTINUE
WRITE(6,7778) (ZT(J,K),J=21,38)
7005 CONTINUE
DO 7002 K=2,KM
FK = K-.5
WRITE(6,7777)
WRITE(6,7001) FK,CD
7001 FORMAT(1X,'VERTICAL VELOCITY AT K = ',F4.1,' DAY ',F7.1)
WRITE(6,890) (THEAD(J),J=3,20)
DO 7003 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=3,20)
7000 FORMAT(1H ,13,1X,18F7.2)
7003 CONTINUE
WRITE(6,7778) (ZW(J,K),J=3,20)
WRITE(6,7777)
WRITE(6,7001) FK,CD
WRITE(6,890) (THEAD(J),J=21,38)
DO 7024 I=IMH,IM
WRITE(6,7000) I,(W(I,J,K),J=21,38)
7024 CONTINUE
WRITE(6,7778) (ZW(J,K),J=21,38)
7778 FORMAT(/30X,'ZONAL MEANS'//5X,18F7.2)
7002 CONTINUE
IF(UV.GT.1.0E26) STOP 792
WRITE(6,7777)
WRITE(6,9016) CD
9016 FORMAT(1X,'SURFACE HEAT FLUX(CAL PER DAY) DAY = ',F7.1/)
WRITE(6,9020) QSH
9020 FORMAT(' GLOBAL MEAN = ',F10.3)
CALL PRINT(QSH,ZSH,THEAD,ICTL,RCTL)
WRITE(6,7777)
WRITE(6,9017)
FORMAT(' LATENT HEAT FLUX')
WRITE(6,9020) QLE
CALL PRINT(QE,ZQE,THEAD,ICTL,RCTL)
WRITE(6,7777)
WRITE(6,9018)
FORMAT(' SENSIBLE HEAT FLUX')
WRITE(6,9020) QOH
CALL PRINT(QH,ZQH,THEAD,ICTL,RCTL)
WRITE(6,7777)

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      WRITE(6,9023)
9023  FORMAT(' SURFACE RADIATION FLUX (CAL/CM**2/DAY) ')
      WRITE(6,9020) GRN
      CALL PRINT(PN,ZRN,THEAD,ICTL,RCTL)
      IF(NN.GE.NPND) GO TO 2501
7019 CONTINUE
      IF(MAT.EQ.0) GO TO 251
      MAT=MAT+1
      IF(MAT.LT.8) GO TO 7017
      DDT=DT*2.0
      GO TO 251
7017 DDT=DT
      IF(MAT.EQ.3) GO TO 20
      IF(MAT.EQ.4) NK=3
      IF(MAT.EQ.5) GO TO 21
      IF(MAT.EQ.6) NK=3
      GO TO 250
20  NK=1
      MAT=7
      NK=3
      GO TO 22
21  NK=2
22  NN=NN+1
      CD=CD+DTD
      GO TO 250
2501 CONTINUE
      DO 3005 J=3,37
      LJ = LV(J)
      DO 3005 M1=1,LJ
      II = LA(M1,J)
39  FORMAT('0',4X,19F6.1/)
      IG = LB(M1,J)
      DO 3005 I=II,IG
      UU(I,J,1) = UU(I,J,1)*Z(1)+UU(I,J,2)*Z(2)+UU(I,J,3)*Z(3)
      X + UU(I,J,4)*Z(4) + UU(I,J,5)*Z(5)
      VV(I,J,1) = VV(I,J,1)*Z(1)+VV(I,J,2)*Z(2)+VV(I,J,3)*Z(3)
      X + VV(I,J,4)*Z(4) + VV(I,J,5)*Z(5)
3005 CONTINUE
3004 FORMAT(' ',I3,1X,19F6.3,1X,I3)
      WRITE(6,7777)
      WRITE(6,3001)
3001 FORMAT(' UUBAR ')
      WRITE(6,89) (UHEAD(J),J=3,21)
      DO 3006 I=3,146
3006 WRITE(6,3004) I,(UU(I,J,1),J=3,21),I
      WRITE(6,89) (UHEAD(J),J=20,38)
      DO 3007 I=3,146
3007 WRITE(6,3004) I,(UU(I,J,1),J=20,38),I
      WRITE(6,7777)
      WRITE(6,3002)
3002 FORMAT(' VVBAR ')
      WRITE(6,89) (UHEAD(J),J=3,21)
      DO 3008 I=3,146
3008 WRITE(6,3004) I,(VV(I,J,1),J=3,21),I
      WRITE(6,89) (UHEAD(J),J=20,38)
      DO 3009 I=3,146
3009 WRITE(6,3004) I,(VV(I,J,1),J=20,38),I
92  STOP
93  REWIND KT
      KT=KT+1
      MAG = 0
      GO TO 7015
END
      SUBROUTINE PRINT(FI,ZSP,THEAD,ICTL,RCTL)
      DIMENSION THEAD(39)
      DIMENSION FIELD(18),ZSP(39),FI(147,39),ICTL(7),RCTL(2)

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1111 FORMAT('11,30X,1X,18F7.2')
7012 FORMAT(11,13,1X,18F7.2)
890 FORMAT(/30X,'ZONAL MEANS'//5X,18F7.2)
7778 WRITE(6,890) (THEAD(J),J=3,20)
      CALL SHADE (ICTL,RCTL,0.)
      DO 9013 I=3,146
      DO 701 J=3,20
      J1 = J-2
101   FIELD(J1) = FI(I,J)
      CALL SHADE(0,0.,FIELD(1))
      WRITE(6,7012) I,FIELD
9013 CONTINUE
      WRITE(6,7778) (ZSP(J),J=3,20)
      WRITE(6,7777)
      WRITE(6,890) (THEAD(J),J=21,38)
      CALL SHADE (ICTL,RCTL,0.)
      DO 9015 I=3,146
      DO 702 J=21,38
      J1 = J-20
702   FIELD(J1) = FI(I,J)
      CALL SHADE(0,0.,FIELD(1))
      WRITE(6,7012) I,FIELD
9015 CONTINUE
      WRITE(6,7778) (ZSP(J),J=21,38)
      RETURN
      END

      SUBROUTINE ADJUST
      COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XBT(38),XHS(38),
3 XMY(38), Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHRR,AH2,BB,BE2,AAA,BBE,DDT,A1,UU,
5UUU,VVV,RRH,AQ,GAM2,AL2,BUN,RY,AM,AMHR,GAMGAM,ALAL,RAN,KMP1,
6MPP(147,39),MQQ(147,39),TM,JM,KM,IMM1,JMM1,KMM1,IMP1,JMP1,MAT,
7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
8LA(10,39),LB(10,39),NN,TE(147,46),UN(147,39),TD(147,46),RN(147,39)
*,CL(147,39)
      MR=0
41 KP1=1
      MAR=0
40 IF(KP1.EQ.KM) GO TO 50
      K=KP1
      KP1=K+1
      B=(AT(K)-AT(KP1))/(ABS(AT(K)))
      IF(B.GE.-5.0E-6) GO TO 40
      DZ1=Z(K)
      DZ2 = Z(KP1)
      AVT=(AT(KP1)*DZ2+AT(K)*DZ1)/(DZ2+DZ1)
      AT(KP1)=AVT
      AT(K)=AVT
      MAR=1
      GO TO 40
50 IF(MAR.EQ.0) GO TO 51
      MR=MR+1
      IF(MR.LT.1000) GO TO 41
      WRITE(6,1) (AT(J),J=1,KM)
1   FORMAT(1H ,23HTOO MANY OPER IN ADJUST,5E15.7)
51 RETURN
      END

      SUBROUTINE EQA
      COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XBT(38),XPS(38),
3 XMY(38), Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHRR,AH2,BB,BE2,AAA,BBE,DDT,A1,PV,
```

DUUU, VVV, RRH, AQ, GAAZ, ALZ, DUN, R1, BN, AMPH, GANGAI, ALAL, KAN, KELI,
 6MPP (147, 39), MOO (147, 39), TM, JM, KM, IMP1, JMM1, KMM1, IMP1, JMP1, MAT,
 7 NK, NNNN, IMH, JMH, MATS, L (39), KA (10, 39), KB (10, 39), LV (39), WFND,
 8LA (10, 39), LB (10, 39), NN, TE (147, 46), UN (147, 39), TD (147, 46), PN (147, 39)
 *, CL (147, 39)

```

  DIMENSION SEN (147, 39, 5)
  EQUIVALENCE (W(1), SEN(1))
  COMMON/TEMP/TEN(146, 38, 5)
  DO 3000 J=JMH, JMM1
  JP1=J+1
  JM1=J-1
  XMJ=XM(J)
  XMJ1=XM(JM1)
  XJ=X(J)
  XJP1=X(JP1)
  XJ1=X(JM1)
  AD=A1*XJ/XMJ*0.3
  AC=A1*XJP1/XMJ*0.3
  AB=AMRR/(XMJ*XMJ)*0.3
  RXMJ=R*XMJ
  LJ=LV(J)
  DO 4002 M1=1, LJ
  II=LA(M1, J)
  IG=LB(M1, J)
  DO 3001 I=II, IG
  MQ=MQQ(I, J)
  IP1=I+1
  IM1=I-1

```

C*****COMPUTATION OF PRESSURE
 GO TO (1, 2, 3), NK

3 CONTINUE

```

  SP0=SP(I, J)-SP(IP1, JP1)
  SP1=SP(IP1, J)-SP(I, JP1)
  PYBIJ=SP1-SP0
  PYBIJ=-SP1-SP0
  GO TO 4
  1 PXBIJ=(SP(IP1, JP1)-SP(I, JP1))*2.0
  PYBIJ=(SP(IP1, JP1)-SP(IP1, J))*2.0
  GO TO 4
  2 PXBIJ=(SP(IP1, J)-SP(I, J))*2.0
  PYBIJ=(SP(I, JP1)-SP(I, J))*2.0
  4 CONTINUE

```

C*****COMPUTATION OF PRESSURE

```

  WEIJ=WE(I, J)
  WNIJ=WN(I, J)
  DO 3002 K=1, KM
  KP1=K+1
  ZK=Z(K)
  ZZ1=ZZ(KP1)
  KM1=K-1
  ZZK=ZZ(K)

```

5555 HS=V(I, J, K)
 HT=U(I, J, K)
 UM1J=U(IM1, J, K)
 VM1J=V(IM1, J, K)
 UP1J=U(IP1, J, K)
 VP1J=V(IP1, J, K)
 UIP1=U(I, JP1, K)
 VIP1=V(I, JP1, K)
 UIM1=U(I, JM1, K)
 VIM1=V(I, JM1, K)

5556 DIJ=HT
 VIJ=HS
 AX=AZHH/ZK
 IF(K.EQ.1) GO TO 3003
 DUZ=(U(I, J, KM1)-HT)/7ZK

DVZ= (V(I,J,KM1)-HS)/ZK
IF(K.NE.KM) GO TO 3004
DUZP1=0.0
DVZP1=0.0
GO TO 3009

3003 DUZ=WEIJ
DVZ=WNIJ

3004 DUZP1=(HT-U(I,J,KP1))/ZZ1
DVZP1=(HS-V(I,J,KP1))/ZZ1
HT=AX*(DUZ-DUZP1-WEIJ*ZK)
HS=AX*(DVZ-DVZP1-WNIJ*ZK)
IF(MQ.EQ.1) GO TO 3008
IF(MQ.EQ.1211) GO TO 1211
IF(MQ.EQ.1112) GO TO 1112
IF(MQ.EQ.1121) GO TO 1121
IF(MQ.EQ.2211) GO TO 2211
IF(MQ.EQ.2112) GO TO 2112
IF(MQ.EQ.1221) GO TO 1221
IF(MQ.EQ.1122) GO TO 1122
IF(MQ.EQ.2121) GO TO 2121
IF(MQ.EQ.1212) GO TO 1212
IF(MQ.EQ.2221) GO TO 2221
IF(MQ.EQ.2212) GO TO 2212
IF(MQ.EQ.1222) GO TO 1222
IF(MQ.EQ.2122) GO TO 2122

2111 UP1J=-UIJ
VP1J=-VIJ
GO TO 3008

1211 UIP1=-UIJ
VIP1=-VIJ
GO TO 3008

1121 UM1J=-UIJ
VM1J=-VIJ
GO TO 3008

1112 VIM1=-VIJ
UIM1=-UIJ
GO TO 3008

2221 UP1J=-UIJ
VP1J=-VIJ
UIP1=-UIJ
VIP1=-VIJ
UM1J=-UIJ
VM1J=-VIJ
GO TO 3008

2212 UP1J=-UIJ
VP1J=-VIJ
VIP1=-VIJ
UIP1=-UIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008

1222 UIP1=-UIJ
VIP1=-VIJ
UM1J=-UIJ
VM1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008

2222 UP1J=-UIJ
VP1J=-VIJ
UM1J=-UIJ
VM1J=-VIJ
UIM1=-UIJ
VIM1=-VIJ
GO TO 3008

2211 UP1J=-UIJ

VP1J=-VIJ
 VIP1=-VIJ
 VIP1=-VIJ
 GO TO 3008
2121 UP1J=-UIJ
 VP1J=-VIJ
 UM1J=-UIJ
 VM1J=-VIJ
 GO TO 3008
2112 UP1J=-UIJ
 VP1J=-VIJ
 UIM1=-UIJ
 VIM1=-VIJ
 GO TO 3008
1221 UIP1=-UIJ
 VIP1=-VIJ
 UM1J=-UIJ
 VM1J=-VIJ
 GO TO 3008
1212 UIP1=-UIJ
 VIP1=-VIJ
 UIM1=-UIJ
 VIM1=-VIJ
 GO TO 3008
1122 UM1J=-UIJ
 VM1J=-VIJ
 UIM1=-UIJ
 VIM1=-VIJ
 GO TO 3008
3008 HT=HT+AB*(UP1J+UM1J-2.0*UIJ)+AC*(UIP1-UIJ)-AD*(UJJ-UIM1)
 HS=HS+AB*(VP1J+VM1J-2.0*VIJ)+AC*(VIP1-VIJ)-AD*(VJJ-VIM1)
 IF(K.NE.1) GO TO 4000
 PA=0.0
 PB=0.0
 GO TO 4001
4000 GO TO (5,6,7),NK
 5 PA=PA+Z2K* ALAL*(T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1))
 PB=PB+Z2K* ALAL*(T(IP1,J,K)+T(IP1,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1))
 GO TO 4001
 6 PA=PA+Z2K* ALAL*(T(I,J,K)+T(I,J,KM1)-T(IP1,J,K)-T(IP1,J,KM1))
 PB=PB+Z2K* ALAL*(T(I,J,K)+T(I,J,KM1)-T(IP1,JP1,K)-T(I,JP1,KM1))
 GO TO 4001
7 CONTINUE
 P1=T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,J,K)-T(IP1,J,KM1)
 P2=T(I,J,K)+T(I,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1)
 PA=PA+Z Z K * AL*(P1+P2)
 PB=PB+Z Z K * AL*(P2-P1)
4001 TEN(I,J,K)=((-PA*AQ+PXBIJ)/R XMJ +HT)*DDT
 SEN(I,J,K)=((-PB*AQ+PYBIJ)/R Y +HS)*DDT
3002 CONTINUE
3001 CONTINUE
4002 CONTINUE
3000 CONTINUE
 UUU=0.0
 VVV=0.0
 IF(MAT.EQ.0) GO TO 3010
 IF(MAT.EQ.((MAT/2)*2)) GO TO 3012
 IF(MAT.EQ.1) GO TO 3013
C MAT=3,5,7
3011 READ(3) U,V
 REWIND 3
 DO 3106 J=JMH,JMM1
 XJ1=XJA(J)/2.0
 HT=1.0/(1.0+XJ1**2)
 HS=YHS(J)/2.0

```

      LJ=LV(J)
      DO 4005 M1=1,LJ
      II=LA(M1,J)
      IG=LB(M1,J)
      DO 3107 I=II,IG
      DO 3108 K=1,KM
      VL=XMJN*Z(K)
      AIJ=U(I,J,K)
      BIJ=V(I,J,K)
      AUZ=AIJ+TEN(I,J,K)+HS*BIJ
      AVZ=BIJ+SEN(I,J,K)-HS*AIJ
      P1=(AUZ+XJ1*AVZ)*HT
      P2=(AVZ-XJ1*AUZ)*HT
      UU(I,J,K)=P1
      VV(I,J,K)=P2
      UUU=UUU+P1*P1*VL
      VVV=VVV+P2*P2*VL
3108 CONTINUE
3107 CONTINUE
4005 CONTINUE
3106 CONTINUE
10 DO 8 K=1,KM
     DO 12 J=JMH,JMM1
     UU(2,J,K)=UU(1M,J,K)
     VV(2,J,K)=VV(1M,J,K)
     UU(1MP1,J,K)=UU(3,J,K)
     VV(1MP1,J,K)=VV(3,J,K)
12 CONTINUE
8 CONTINUE
     READ(2) T
     REWIND 2
     IF(MAT.EQ.7) GO TO 3120
     WRITE(3) UU,VV
     REWIND 3
     DO 3999 K=1,KM
     DO 3998 J=JMH,JMM1
     DO 3997 T=1,IMP1
     U(I,J,K)=UU(I,J,K)
     V(I,J,K)=VV(I,J,K)
3997 CONTINUE
3998 CONTINUE
3999 CONTINUE
     GO TO 11
C     MAT=1
3013 DO 3100 J=JMH,JMM1
     LJ=LV(J)
     XJ1=XJA(J)
     HT=XHT(J)
     HS=XHS(J)
     XMJN=XMY(J)
     DO 4003 M1=1,LJ
     II=LA(M1,J)
     IG=LB(M1,J)
     DO 3101 I=II,IG
     DO 3102 K=1,KM
     VL=XMJN*Z(K)
     AIJ=U(I,J,K)
     BIJ=V(I,J,K)
     AUZ=AIJ +TEN(I,J,K)+HS*BIJ
     AVZ=BIJ+SEN(I,J,K)-HS*AIJ
     AIJ=(AUZ+XJ1*AVZ)*HT
     BIJ=(AVZ-XJ1*AUZ)*HT
     UU(I,J,K)=AIJ
     VV(I,J,K)=BIJ
     UUU=UUU+ATJ*AIJ*VL

```

3102 CONTINUE
 3101 CONTINUE
 4003 CONTINUE
 3100 CONTINUE
 GO TO 10
 C MAT=2,4,6
 12 DO 3103 J=JMH,JMM1
 XJ1=XJA(J)/2.0
 HT=1.0/(1.0+XJ1*XJ1)
 HS=XHS(J)/2.0
 LJ=LV(J)
 XMJN=XMY(J)
 DO 4004 M1=1,LJ
 II=LA(M1,J)
 IG=LB(M1,J)
 DO 3104 I=II,IG
 DO 3105 K=1,KM
 VL=XMJN*Z(K)
 AIJ=U(I,J,K)
 BIJ=V(I,J,K)
 AUZ=AIJ+TEN(I,J,K)+HS*BIJ
 AVZ=BIJ+SEN(I,J,K)-HS*AIJ
 P1=(AUZ+XJ1*AVZ)*HT
 P2=(AVZ-XJ1*AUZ)*HT
 U(I,J,K)=P1
 UU(I,J,K)=P1
 V(I,J,K)=P2
 VV(I,J,K)=P2
 UUU=UUU+P1*P1*VL
 VVV=VVV+P2*P2*VL
 3105 CONTINUE
 3104 CONTINUE
 4004 CONTINUE
 3103 CONTINUE
 DO 3113 K=1,KM
 DO 3114 J=JMH,JM
 DO 3115 I=2,IMP1
 T(I,J,K)=TT(I,J,K)
 3115 CONTINUE
 3114 CONTINUE
 3113 CONTINUE
 GO TO 3120
 C MAT=0
 3010 DO 3109 J=JMH,JMM1
 XJ1=XJA(J)
 HT=XHT(J)
 HS=XHS(J)
 XMJN=XMY(J)
 LJ=LV(J)
 DO 4006 M1=1,LJ
 II=LA(M1,J)
 IG=LB(M1,J)
 DO 3110 I=II,IG
 DO 3111 K=1,KM
 VL=Z(K)*XMJN
 AIJ=U(I,J,K)
 BIJ=V(I,J,K)
 U(I,J,K)=UU(I,J,K)
 V(I,J,K)=VV(I,J,K)
 AUZ=AIJ+TEN(I,J,K)+HS*BIJ
 AVZ=BIJ+SEN(I,J,K)-HS*AIJ
 P1=(AUZ+XJ1*AVZ)*HT
 P2=(AVZ-XJ1*AUZ)*HT
 UU(I,J,K)=P1
 VV(I,J,K)=P2

UUU=UUU+P1*P1*VL
 VVV=VVV+P2*P2*VL

3111 CONTINUE
 3110 CONTINUE
 4006 CONTINUE
 3109 CONTINUE
 320 CONTINUE
 DO 4007 K=1,KM
 DO 4008 J=JMH,JMM1
 U(2,J,K)=U(IM,J,K)
 V(2,J,K)=V(IM,J,K)
 UU(2,J,K)=UU(IM,J,K)
 VV(2,J,K)=VV(IM,J,K)
 U(TMP1,J,K)=U(3,J,K)
 V(TMP1,J,K)=V(3,J,K)
 UU(TMP1,J,K)=UU(3,J,K)
 VV(TMP1,J,K)=VV(3,J,K)

4008 CONTINUE
 4007 CONTINUE
 11 UUU=UUU*FRH
 VVV=VVV*RRH
 UV=UUU+VVV
 RETURN
 END
 SUBROUTINE CONTI
 COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
 1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),WB(147,39),
 2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XHT(38),XHS(38),
 3 XMY(38),Z(5),X(39),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
 4GAM,Y,YY,R,RR,HH,H2,AHY,AHPR,AH2,BB,BB2,AAA,BBE,DDT,A1,UV,
 5UUU,VVV,RRH,AQ,GAM2,AL2,BUN,RY,AM,AMRR,GAMGAM,ALAL,BAN,KMP1,
 6MPP(147,39),MQO(147,39),IM,JM,KM,IMM1,JMM1,KMM1,TMP1,JMP1,MAT,
 7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
 8LA(10,39),LB(10,39),NN,TF(147,46),UN(147,39),TD(147,46),PN(147,39)
 *,CL(147,39)
 DIMENSION WWW(10)

5 DO 1000 J=3,JM
 XJ=X(J)
 JM1=J-1
 XMJ=XM(J)
 XM1=XM(J+1)
 WT=1.0/(XJ*Y)
 B=XMJ*WT
 CCC=XM1*WT
 LJ=L(J)
 DO 1 M1=1,LJ
 II=KA(M1,J)
 IG=KB(M1,J)
 DO 1001 I=II,IG
 MP=MPP(I,J)
 IM1=I-1
 IF(MP.EQ.1) GO TO 1200

1999 IF(MP.EQ.11) GO TO 1011
 IF(MP.EQ.12) GO TO 1012
 IF(MP.EQ.13) GO TO 1013
 IF(MP.EQ.14) GO TO 1014
 IF(MP.EQ.21) GO TO 1021
 IF(MP.EQ.22) GO TO 1022
 IF(MP.EQ.23) GO TO 1023
 IF(MP.EQ.24) GO TO 1024
 IF(MP.EQ.31) GO TO 1031
 IF(MP.EQ.32) GO TO 1032
 IF(MP.EQ.34) GO TO 1034

1033 DO 1113 K=1,KMM1
 WWW(K)=((UU(I,J,K)+UU(I,JM1,K)-UU(IM1,J,K))/XJ
 1+(VV(I,J,K)+VV(TM1,J,K))*P1-VV(I,JM1,K)*CCC)*PAN*Z(K)

1113 CONTINUE
 GO TO 1998
 1200 DO 1003 K=1,KMM1

$$WWW(K) = (((UU(I,J,K)+UU(I,JM1,K)-UU(IM1,J,K)-UU(IM1,JM1,K))/XJ -$$

$$1+(VV(I,J,K)+VV(IM1,J,K))*B-(VV(T,JM1,K)+VV(IM1,JM1,K))*CCC)/2.0$$

$$2)*Z(K)$$

1003 CONTINUE
 GO TO 1998
 1011 DO 1004 K=1,KMM1

$$WWW(K) = ((-UU(IM1,J,K)+UU(IM1,JM1,K))/XJ+VV(IM1,J,K)*B$$

$$-VV(IM1,JM1,K)*CCC)*Z(K)$$

1004 CONTINUE
 GO TO 1998
 1012 DO 1005 K=1,KMM1

$$WWW(K) = ((UU(I,JM1,K)-UU(IM1,JM1,K))/XJ-$$

$$1(VV(I,JM1,K)+VV(IM1,JM1,K))*CCC)*Z(K)$$

1005 CONTINUE
 GO TO 1998
 1013 DO 1006 K=1,KMM1

$$WWW(K) = ((UU(I,J,K)+UU(I,JM1,K))/XJ+VV(I,J,K)*B-VV(I,JM1,K)*CCC)*$$

$$Z(K)$$

1006 CONTINUE
 GO TO 1998
 1014 DO 1007 K=1,KMM1

$$WWW(K) = ((UU(I,J,K)-UU(IM1,J,K))/XJ+(VV(I,J,K)+VV(IM1,J,K))*B)*Z(K)$$

1007 CONTINUE
 GO TO 1998
 1021 DO 1008 K=1,KMM1

$$WWW(K) = (-UU(IM1,JM1,K)/XJ-VV(IM1,JM1,K)*CCC)*2.0*Z(K)$$

1008 CONTINUE
 GO TO 1998
 1022 DO 1009 K=1,KMM1

$$WWW(K) = (UU(I,JM1,K)/XJ-VV(I,JM1,K)*CCC)*2.0*Z(K)$$

1009 CONTINUE
 GO TO 1998
 1023 DO 1109 K=1,KMM1

$$WWW(K) = 2.0*Z(K)*(UU(I,J,K)/XJ + VV(I,J,K)*B)$$

1109 CONTINUE
 GO TO 1998
 1024 DO 1110 K=1,KMM1

$$WWW(K) = 2.0*Z(K)*(-UU(IM1,J,K)/XJ + VV(IM1,J,K)*B)$$

1110 CONTINUE
 GO TO 1998
 1031 DO 1111 K=1,KMM1

$$WWW(K) = ((UU(I,JM1,K)-UU(IM1,J,K)-UU(IM1,JM1,K))/XJ+VV(IM1,J,K)*B$$

$$-1-(VV(I,JM1,K)+VV(IM1,JM1,K))*CCC)*BAN*Z(K)$$

1111 CONTINUE
 GO TO 1998
 1032 DO 1112 K=1,KMM1

$$WWW(K) = ((UU(I,J,K)+UU(T,JM1,K)-UU(IM1,JM1,K))/XJ$$

$$-1-(VV(IM1,JM1,K)+VV(I,JM1,K))*CCC+VV(I,J,K)*B)*BAN*Z(K)$$

1112 CONTINUE
 GO TO 1998
 1034 DO 1114 K=1,KMM1

$$WWW(K) = ((UU(I,J,K)-UU(IM1,JM1,K)-UU(IM1,J,K))/XJ$$

$$1+(VV(I,J,K)+VV(IM1,J,K))*B-VV(IM1,JM1,K)*CCC)*BAN*Z(K)$$

1114 CONTINUE
 98 WT=0.0
 DO 1997 K=1,KMM1

$$W1=WT+WWW(K)$$

$$W(I,J,K+1)=W1$$

$$WT=W1$$

1997 CONTINUE
 1001 CONTINUE
 1 CONTINUE
 1000 CONTINUE

RETURN
 END
 SUBROUTINE THERM
 COMMON T(147,39,5), TT(147,39,5), SP(147,39), AT(5), UU(147,39,5),
 UV(147,39,5), U(147,39,5), V(147,39,5), W(147,39,5), UW(147,39),
 VVB(147,39), WE(147,39), WN(147,39), Q(39), XJA(38), XHT(38), XHS(38),
 Z(XMY(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, A2, AH, DT, AL,
 4GAM, Y, YY, R, RP, HH, B2, AZBH, B2, AHY, AHFR, AH2, BB, BB2, MAB, RBE, DDT, A1, UV,
 5HUU, VVV, RRH, AQ, GAM2, AL2, BUN, RY, AM, AMRF, GAMGAM, ALAL, EAN, KMP1,
 6MPP(147,39), MQQ(147,39), TM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,
 7 NK, NNNN, IMH, JMH, MATS, L(39), KA(10,39), KB(10,39), LV(39), NEND,
 8LA(10,39), LB(10,39), UN, TE(147,46), UN(147,39), TD(147,46), RN(147,39)
 *, CL(147,39)
 COMMON/T/TEMP/T/PN(147,39,5)
 HG=H*490.0
 IF(MAT.NE.8) GO TO 6
 MAT=0
 WRITE(6,234) NN
 234 FORMAT(1H ,3HEND,4X,5HTIME=I6)
 6 CONTINUE
 SBC=8.3E-11*0.01666
 DO 20 J=JMH, JM
 JM1=J-1
 QJ=Q(J)
 XJ=X(J)
 JP1=J+1
 AA=1.0/(R2*XJ)
 AA2=AA/2.0
 XJ1=X(JM1)
 XMJ=XM(J)
 XMJ1=XM(JM1)
 BB2=XMJ*AA2/Y
 AH22=AH2*XMJ/XJ
 BB1=BB2*2.0
 CC2=XMJ1*AA2/Y
 CC=CC2*2.0
 AHM=AH Y/XJ
 AH1=AHRR/(XJ*XJ)
 AH3=AH2*XMJ1/X J
 LJ=L(J)
 DO 4011 M1=1, LJ
 II=KA(M1,J)
 IG=KB(M1,J)
 DO 21 I=II, IG
 UM=UN(I,J)*51.48
 TEIJ=TE(I,J)
 CLN=CL(I,J)*0.125
 MP=MPP(I,J)
 RSN=QJ*(1.-0.7*CLN)
 *****COMPUTATION OF PRESSURE*****
 PZ=0.0
 PZ1=0.0
 DO 4018 K=1, KMM1
 KP1=K+1
 PZ=PZ-ZZ(KP1)*AL2*(TT(I,J,K)+TT(I,J,KP1))
 PZ1=PZ1+PZ*Z(KP1)
 4018 CONTINUE
 SP(I,J)=PZ1*HG
 IP1=J+1
 IM1=I-1
 UETJ=UB(I,J)
 UBM1J=UB(IM1,J)
 UBIM1=UR(I,JM1)
 VBIJ=VB(I,J)
 VBM1J=VB(IM1,J)
 VBIM1=VB(I,JM1)

UBM1=U-BB(I,J1,JM1)
 VBM1M1=VB(I,M1,JM1)
 TA=TE(I,J)+273.15
 TW=TD(I,J)+273.15
 123 TS=T(I,J,1)+273.15
 PCB=1013.25*0.1
 ESS=10.0** (8.4051-2353.0/TS)
 ESD=10.0** (8.4051-2353.0/TW)
 RLN=SBC*TS**4*0.985*(0.39-0.05*SQRT(ESD*10.))*(1.-0.6*CLN**2)
 RNS=RSN-RLN
 RN(I,J)=RNS
 QS=0.622*ESS/(PCB-ESS)
 QA=0.622*ESD/(PCB-ESD)
 DO 22 K=1,KM
 KP1=K+1
 ZZ1=ZZ(KP1)
 ZZK=ZZ(K)
 ZK=Z(K)
 C VERTICAL DIFFUSION(HT,HS) AND VERTICAL ADVECTION(WT,WS)
 WIJ=W(J,J,K)
 CC1=1.0/(R2*ZK)
 KM1=K-1
 TTP1J=TT(IP1,J,K)
 TTM1J=TT(IM1,J,K)
 TTIP1=TT(I,JP1,K)
 TTIM1=TT(I,JM1,K)
 TTIJ=TT(I,J,K)
 TIJ=T(I,J,K)
 IF(K.EQ.1.AND.((TIJ-TTIJ)+0.609*TS*(QS-QA)).GE.0.0) GO TO 333
 IF(K.EQ.1) GO TO 334
 TXIJ=(T(I,J,KM1)-TIJ)/ZZK
 WT=(TTIJ+TT(I,J,KM1))*WIJ
 IF(K.NE.KM) GO TO 2003
 TYIJ=0.0
 PK=0.0
 PK1=0.0
 GO TO 2004
 333 CU=0.033
 CO=1.23*0.001
 GO TO 133
 334 CU=0.018
 CO=0.41*0.001
 -133 QH=1.2*0.001*0.24*CO*UM*(TIJ-TTIJ)
 QE=1.2*0.001*CO*595.*UM*(QS-QA)
 TXIJ=(RNS-QH-QE)*H/AZ
 WT=0.0
 2003 TYIJ=(TIJ-T(I,J,KP1))/ZZ1
 WIJP=W(T,J,KP1)
 PK=(TTIJ+TT(I,J,KP1))*WIJP
 2004 HS=AZHH/ZK
 WT=(WT-PK)*CC1
 HT=HS*(TXIJ-TYIJ)
 C HORIZONTAL DIFFUSION(HT,HS) AND HORIZONTAL ADVECTION(WT,WS)
 TXIJ=(T(IP1,J,K)-TIJ)*AH1
 TXM1J=(TIJ-T(IM1,J,K))*AH1
 TYIJ=(T(I,JP1,K)-TIJ)*AH22
 TYIM1=(TIJ-T(I,JM1,K))*AH3
 VIJ=VV(I,J,K)+VBIJ
 VM1J=VV(IM1,J,K)+VBM1J
 VIM1=VV(I,JM1,K)+VBIM1
 VM1M1=VV(IM1,JM1,K)+VBM1M1
 UIJ=UU(I,J,K)+UBIJ
 UM1J=UU(IM1,J,K)+UBM1J
 UIM1=UU(I,JM1,K)+UBIM1
 UM1M1=UU(IM1,JM1,K)+UBM1M1
 TF(MP.EQ.1) GO TO 2001

IF(MP.EQ.11) GO TO 2011
 IF(MP.EQ.12) GO TO 2012
 IF(MP.EQ.13) GO TO 2013
 IF(MP.EQ.14) GO TO 2014
 IF(MP.EQ.21) GO TO 2021
 IF(MP.EQ.23) GO TO 2023
 IF(MP.EQ.24) GO TO 2024
 IF(MP.EQ.31) GO TO 2031
 IF(MP.EQ.32) GO TO 2032
 IF(MP.EQ.34) GO TO 2034
 IF(MP.EQ.22) GO TO 2022
2033 F=UIJ+UIM1
 G=(VIJ+VM1J)*BB2
 FF=VIM1*CC2
 WT=WT+((TTIJ+TTP1J)*F -(TTIJ+TTM1J)*UM1J)*AA2+
 1*(TTIJ+TTIP1)*G -(TTIJ+TTIM1)*FF)*BUN
 HT=HT+(TXIJ+TYIJ-(TXM1J+TYIM1)/2.0)*BUN
 GO TO 2005
2001 F=UIJ+UIM1
 G=(VIJ+VM1J)*BB2
 FF=UM1J+UM1M1
 GG=(VIM1+VM1M1)*CC2
 WT=WT+((TTIJ+TTP1J)*F -(TTIJ+TTM1J)*FP)*AA2
 1*(TTIJ+TTIP1)*G -(TTIJ+TTIM1)*GG
 HT=TXIJ-TXM1J+TYIJ-TYIM1+HT
 GO TO 2005
2011 F=(UM1M1+UM1J)*AA
 G=VM1J*BB1
 FF=VM1M1*CC
 WT=WT-(TTIJ+TTM1J)*F + (TTIJ+TTIP1)*G
 1-(TTIJ+TTIM1)*FF
 HT=-TXM1J*2.0+TYIJ-TYIM1+HT
 GO TO 2005
2012 F=(VIM1+VM1M1)*CC
 WT=WT+((TTIJ+TTP1J)*UIM1-(TTIJ+TTM1J)*UM1M1)*AA
 1-(TTIJ+TTIM1)*F
 HT=TXIJ-TXM1J-TYIM1*2.0+HT
 GO TO 2005
2013 F=(UIJ+UIM1)*AA
 G=VIJ*BB1
 FF=VIM1*CC
 WT=WT+((TTIJ+TTP1J)*F +(TTIJ+TTIP1)*G
 1-(TTIJ+TTIM1)*FF
 HT=TXIJ*2.0+TYIJ-TYIM1+HT
 GO TO 2005
2014 F=(VIJ+VM1J)*BB1
 WT=WT+((TTIJ+TTP1J)*UIJ-(TTIJ+TTM1J)*UM1J)*AA
 1*(TTIJ+TTIP1)*F
 HT=TXIJ-TXM1J+TYIJ*2.0+HT
 GO TO 2005
2021 F=UM1M1*AA
 G=VM1M1*CC
 WT=WT-(TTIJ+TTM1J)*F *2.0-(TTIJ+TTIM1)*G *2.0
 HT=HT-(TXM1J+TYIM1)*2.0
 GO TO 2005
2022 F=UIM1*AA
 G=VIM1*CC
 WT=WT+((TTIJ+TTP1J)*F -(TTIJ+TTIM1)*G)*2.0
 HT=(TXIJ-TYIM1)*2.0+HT
 GO TO 2005
2023 F=UIJ*AA
 G=VIJ*BB1
 WT=WT+((TTIJ+TTP1J)*F +(TTIJ+TTIP1)*G)*2.0
 HT=(TXIJ+TYIJ)*2.0+HT
 GO TO 2005
2024 F=UM1J*AA

G=V M 1 J + D U J
 WT=WT-((TTI J+TTM1 J)*F - (TTI J+TTIP1)*G) *2.0
 HT=(TYI J-TXM1 J)*2.0+HT
 GO TO 2005

2031 F=UM1M1+UM1J
 G=VM1J*BB2
 FF=(VIM1+VM1M1)*CC2
 WT=WT+((TTI J+TTP1 J)*UI M1-(TTI J+TTM1 J)*F) *AA2+
 1 (TTI J+TTIP1)*G -(TTI J+TTIM1)*FF) *BUN
 HT=((TXI J+TYI J)/2.0-TXM1 J-TYIM1)*BUN+HT
 GO TO 2005

2032 F=UIM1+UIJ
 G=VIJ*BB2
 FF=(VIM1+VM1M1)*CC2
 WT=WT+((TTI J+TTP1 J)*F -(TTI J+TTM1 J)*UM1M1)*AA2+
 1 (TTI J+TTIP1)*G -(TTI J+TTIM1)*FF) *BUN
 HT=((TYI J-TXM1 J)/2.0+TXI J-TYIM1)*BUN+HT
 GO TO 2005

2034 G=(VIJ+VM1J)*BB2
 F=VM1M1*CC2
 FF=UM1J+UM1M1
 WT=WT+((TTI J+TTP1 J)*UIJ-(TTI J+TTM1 J)*FF) *AA2+
 1 (TTI J+TTIP1)*G -(TTI J+TTIM1)*F) *BUN
 HT=((TXI J-TYIM1)/2.0-TXM1 J+TYI J)*BUN+HT

2005 TEN(I,J,K)=DDT*(HT-WT/0.93)
 22 CONTINUE
 21 CONTINUE

4011 CONTINUE
 20 CONTINUE
 IF(MAT.EQ.0) GO TO 2036
 IF(MAT.EQ.(MAT/2)*2)) GO TO 2037
 IF(MAT.EQ.1) GO TO 2038
 MAT=3,5,7

2035 READ(2) TT
 REWIND 2
 DO 38 J=JMH, JM
 LJ=L(J)
 DO 40 14 M1=1,LJ
 II=KA(M1,J)
 IG=KB(M1,J)
 DO 39 I=II,IG
 DO 40 K=1,KM
 AT(K)=TT(I,J,K)+TEN(I,J,K)

40 CONTINUE
 CALL ADJUST
 DO 41 K=1,KM
 TT(I,J,K)=AT(K)

41 CONTINUE
 39 CONTINUE

4014 CONTINUE
 38 CONTINUE
 IF(MAT.EQ.7) GO TO 2500

9 DO 2 K=1,KM
 DO 3 J=JMH, JM
 TT(IMP1,J,K)=TT(3,J,K)
 TT(2,J,K)=TT(1M,J,K)
 T(2,J,K)=T(1M,J,K)
 T(IMP1,J,K)=T(3,J,K)

3 CONTINUE
 2 CONTINUE
 WRITE(2) TT
 REWIND 2
 GO TO 10
 MAT=1

2038 DO 30 J=JMH, JM
 LJ=L(J)

```

DO 4012 M1=1, LJ
II=KA(M1,J)
IG=KB(M1,J)
DO 31 I=II, IG
DO 32 K=1, KM
AT(K)=T(I,J,K)+TEN(I,J,K)
32 CONTINUE
CALL ADJUST
DO 33 K=1, KM
T(I,J,K)=TT(I,J,K)
TT(I,J,K)=AT(K)
33 CONTINUE
31 CONTINUE
4012 CONTINUE
30 CONTINUE
GO TO 9
C      MAT=2,4,6
2037 DO 34 J=JMH,JM
LJ=L(J)
DO 4013 M1=1, LJ
II=KA(M1,J)
IG=KB(M1,J)
DO 35 I=II, IG
DO 36 K=1, KM
AT(K)=T(I,J,K)+TEN(I,J,K)
36 CONTINUE
CALL ADJUST
DO 37 K=1, KM
TT(I,J,K)=AT(K)
37 CONTINUE
35 CONTINUE
4013 CONTINUE
34 CONTINUE
GO TO 2500
C      MAT=0
2036 DO 42 J=JMH,JM
LJ=L(J)
DO 4015 M1=1, LJ
II=KA(M1,J)
IG=KB(M1,J)
DO 43 I=II, IG
DO 44 K=1, KM
AT(K)=T(I,J,K)+TEN(I,J,K)
44 CONTINUE
CALL ADJUST
DO 45 K=1, KM
T(I,J,K)=TT(I,J,K)
TT(I,J,K)=AT(K)
45 CONTINUE
43 CONTINUE
4015 CONTINUE
42 CONTINUE
2500 CONTINUE
DO 4016 K=1, KM
DO 4017 J=JMH,JM
T(2,J,K)=T(IM,J,K)
TT(2,J,K)=TT(IM,J,K)
T(IMP1,J,K)=T(3,J,K)
TT(IMP1,J,K)=TT(3,J,K)
4017 CONTINUE
4016 CONTINUE
10 DO 4019 J=JMH,JM
SP(IMP1,J)=SP(3,J)
4019 CONTINUE
RETURN
END

```

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781

```

SUBROUTINE PRIP
RETURN
END
SUBROUTINE GEOST
RETURN
END
SUBROUTINE PREPA
RETURN
END
SUBROUTINE SHADE(ICTL,RCTL,BVAL)          00000100
                                             00000120
                                             00000140
                                             00000160
                                             00000180
                                             00000200
                                             00000220
                                             00000240
                                             00000260
                                             00000280
C ****
C CALL SHADE (ICTL, RCTL, RFIELD)          *
C ****
C     ICTL (1) ... CALL CODE                 * 00000300
C         =0 -NORMAL INTRA-FIELD CALL          * 00000320
C             (ONLY RFIELD IS USED, ICTL(2) THRU ICTL(8) AND
C             RCTL ARE IGNORED)                  * 00000340
C         =1 -BEGINNING-OF-FIELD CALL          * 00000360
C             (ONLY ICTL AND RCTL PARAMETERS ARE USED, PFIELD
C             IS IGNORED)                      * 00000380
* 00000400
* 00000420
C     ICTL (2) ... OUTPUT TAPE NUMBER        * 00000440
C     ICTL (3) ... LEFT (SHADE) MARGIN        * 00000460
C     ICTL (4) ... NUMBER OF SHADING LINES    * 00000480
C     ICTL (5) ... NUMBER OF FIELDS           * 00000500
C     ICTL (6) ... FIELD WIDTH                * 00000520
C     ICTL (7) ... DOES THE CALLING PROGRAM PRINT INTEFSPERSED DATA * 00000540
C         =1 -NO                            * 00000560
C         =2 -YES                           * 00000580
C     ICTL (8) ... IGNORED                   * 00000600
* 00000620
C     RCTL (1) ... CYCLE POINT               * 00000640
C     RCTL (2) ... SHADE INTERVAL            * 00000660
* 00000680
C     RFIELD ... ONE DIMENSIONAL VECTOR WITH NUMERIC INFROMATION * 00000700
C             TO BE SHADED                  * 00000720
C ****
C IF (ICTL (1) .NE. 0) GO TO 1000          00000740
XL= (BVAL (1)-CP) /SINT
M2=LM
IF (COND) GO TO 3100
BLIN (LM)= (XL-ALIN (LM)) /VDIVS
3021 DO 3029 K=LF,NF,ISKP
M1=M2+1
M2=M2+IFW
XR= ((BVAL (K)-CP) /SINT-XL) /FW
DO 3029 J=M1,M2
XL=XL+XR
3029 BLIN (J)= (YL-ALIN (J)) /VDIVS
3051 DO 3059 L=1,NSL
3041 DO 3049 K=LM,MR
ALIN (K)=ALIN (K)+BLIN (K)
TBLC=AMOD (ALIN (K),TLEN)+1.
IF (TBLC .LT. 1.) TBLC=TBLC+TLEN
IT=TBLC
3049 CLIN (K+2)=CTBL (IT)
3059 WRITE (NTP,CLIN)
IF (.NOT.DATAL) RETURN
3061 DO 3069 K=LM,MR
3069 ALIN (K)=ALIN (K)+BLIN (K)
RETURN

```

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```

3100 IR (NSHADE) GO TO 2000          0.0001200
COND=.FALSE.
ALIN(LM)=XL                         00001260
3121 DO 3129 K=LF,NF,ISKP           00001280
M1=M2+1                             00001320
M2=M2+IFW                           00001340
XR=((BVAL(K)-CP)/SINT-XL)/FW       00001360
DO 3129 J=M1,M2                     00001380
XL=XL+XR                           00001400
3129 ALIN(J)=XL                     00001420
IF (DATA1) RETURN                   00001440
3141 DO 3149 K=LM,MR               00001460
TBLC=AMOD(ALIN(K),TLEN)+1.         00001480
IF (TBLC .LT. 1.) TBLC=TBLC+TLEN   00001500
IT=TBLC                            00001520
3149 CLIN(K+2)=CTBL(IT)           00001540
WRITE (NTP,CLIN)                   00001560
RETURN                               00001580
2000 IF (FRSTLN) GO TO 2030        00001600
2011 DO 2019 L=1,NSL                00001620
2019 WRITE (NTP,CLIN)               00001640
2030 FRSTLN=.FALSE.                 00001660
RETURN                               1680
C*****CONTINUE*****
1000 CONTINUE
ISKP=ICTL(1)                         00001700
LF=ISKP+1                            00001720
NTP=ICTL(2)                           00001740
LM=ICTL(3)                           00001760
NSL=ICTL(4)                          00001780
NF=ICTL(5)                           00001800
IFW=ICTL(6)                          00001820
DATA1=ICTL(7).NE.1                   00001840
VDIVS=NSL                           00001860
IF (DATA1) VDIVS=VDIVS+1.            00001880
IF (LM.LT.2) LM=2                   00001900
IF (IFW.LT.2) IFW=2                 00001920
FW=IFW                               00001940
NS=(NF-1)/ISKP+1                    00001960
MR=LM+(NS-1)*IFW                   00001980
IF (MR.LE.LL) GO TO 1011            00002000
NF=(LL-LM)/IFW*ISKP+1              00002020
NS=(NF-1)/ISKP+1                    00002040
MR=LM+(NS-1)*IFW                   00002060
00002080
1011 CP=RCTL(1)                     00002100
SINT=RCTL(2)                        00002120
FRSTLN=.TRUE.                       00002140
COND=.TRUE.                          00002160
NSHADE=SINT.EQ.0.                  00002180
IF (.NOT.NSHADE) GO TO 1021        00002200
SINT=1.                             00002220
CP=0.                               00002240
MR=1                                00002260
LM=1                                00002280
00002300
1021 DO 1029 I=1,LM                00002320
1029 CLIN(I+2)=BLANK               00002340
CLIN(1)=LP                           00002360
CLIN(2)=QM                           00002380
CLIN(MR+3)=QM                        00002400
CLIN(MR+4)=RP                        00002420
RETURN                               00002440
DATA LL/132/
DATA TLEN/20.0/, CTBL/1H0,1H,1H1,1H,1H2,1H,1H3,1H,1H4,1H
*, 1H5,1H,1H6,1H,1H7,1H,1H8,1H,1H9,1H/
END

```

SUBROUTINE PRP

DATA: IM, JM, KM, IMH, JMH
 OCEAN SHAPE (SUBROUTINE SHAPE2)
 H, Z(I)
 AZ, AM, AH
 WE, WN (GIVEN FROM CARDS, OR A TAPE OR THE SUBROUTINE WIND)
 Q(J) (HEATING FUNCTION, REFERENCE ATMOSPHERIC TEMPERATURE)
 AT(K) (INITIAL TEMPERATURE)
 UB, VB (GIVEN FROM CARDS, OR A MAGNETIC TAPE, OR THE SUBROUTINE
 BARO)
 BB, AAA, BBB (AAA:GRID SIZE IN LATITUDE, BBB:GRID SIZE IN
 LONGITUDE. BOTH IN DEGREES. BB IS THE LATITUDE CORRESPOND-
 ING TO J=0.)

 COMMON F(147, 39, 5), TT(147, 39, 5), SP(147, 39), AT(5), UU(147, 39, 5),
 1VV(147, 39, 5), U(147, 39, 5), V(147, 39, 5), W(147, 39, 5), UB(147, 39),
 2VB(147, 39), WE(147, 39), WN(147, 39), Q(39), XJA(38), XHT(38), XHS(38),
 3 XHY(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,
 4GAM, Y, YY, R, RR, HH, R2, AZHH, R2, AHY, AHRE, AH2, BB, BB2, AAA, BBB, DDT, A1, UV,
 5UUU, VVV, RRH, AQ, GAM2, AL2, BUN, BY, AM, AMRE, GAMGAM, ALAL, BAN, KMP1,
 6MPP(147, 39), MQQ(147, 39), IM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,
 7 NK, NNNN, IMH, JMH, MATS, L(39), KA(10, 39), KB(10, 39), LV(39), NEND,
 8LA(10, 39), LF(10, 39)
 READ(5, 80) IM, JM, KM, IMH, JMH
 80 FORMAT(5I5)
 JMP1=JM+1
 JMM1=JM-1
 IMP1=IM+1
 IMM1=IM-1
 KMM1=KM-1
 CALL SHAPE2
 CALL SHAPE2
 DO 47 K=1, KM
 DO 48 J=1, JMP1
 DO 49 I=1, IMP1
 UH(I, J, K)=0.0
 VV(I, J, K)=0.0
 W(I, J, K)=0.0
 U(I, J, K)=0.0
 V(I, J, K)=0.0
 TT(I, J, K)=0.0
 T(I, J, K)=0.0
 49 CONTINUE
 48 CONTINUE
 47 CONTINUE
 READ(5, 81) H, (Z(I), I=1, KM)
 81 FORMAT(E15.7, 5F10.2)
 WRITE(6, 13) (Z(I), I=1, KM)
 13 FORMAT(1H , 19 HDEPTHS FOR T, U, V=5F10.5)
 KMP1=KM+1
 ZZ(1)=-2.0*Z(1)
 DO 82 I=2, KM
 ZZ(I)=Z(I-1)-Z(I)
 82 CONTINUE
 ZZ(KMP1)=2.0*(1.0+Z(KM))
 DO 83 I=1, KM
 Z(I)=(ZZ(I)+ZZ(I+1))/2.0
 83 CONTINUE
 WRITE(6, 33) H, (Z(I), I=1, KM)
 33 FORMAT(1H , 2HH=E15.7, 2X, 2HZ=6E15.7)
 WRITE(6, 21) (ZZ(I), I=1, KMP1)
 21 FORMAT(1H , 3HZZ=7E15.7)

```

      READ(5,84) AZ,Aa,AB
  84 FORMAT(3E15.7)
  4567 DO 4568 J=1,39
        DO 4569 I=1,IMP1
          WE(I,J)=0.0
          WN(I,J)=0.0
  4569 CONTINUE
  4568 CONTINUE
    CALL WIND
    CALL WIND
    AL=H/AZ
    DO 2000 J=1,IMP1
    DO 2001 I=1,IMP1
      WE(I,J)=WE(I,J)*AL
      MP=MPP(I,J)
      IF(MP.LE.1) GO TO 2003
      IF(MP.GT.5) GO TO 2003
      DO 2002 K=1,KM
        T(I,J,K)=0.0
        TT(I,J,K)=0.0
        W(I,J,K)=444.444
  2002 CONTINUE
  2003 IF(MQQ(I,J).NE.2) GO TO 2001
    DO 2004 K=1,KM
      U(I,J,K)=333.333
      UU(I,J,K)=333.333
      VV(I,J,K)=444.444
      V(I,J,K)=444.444
  2004 CONTINUE
  2001 CONTINUE
  2000 CONTINUE
    READ(5,5) (Q(J),J=JMH,JM)
  5 FORMAT(12F5.0)
    DO 5094 J=3,38
      READ(5,5095) (AT(K),K=1,KM)
  5095 FORMAT(5F10.2)
    LJ=L(J)
    DO 5096 LL=1,LJ
      IM1=KA(LL,J)
      IP1=KB(LL,J)
      DO 97 I=IM1,IP1
      DO 98 K=1,KM
        T(I,J,K)=AT(K)
        TT(I,J,K)=AT(K)
  98 CONTINUE
  97 CONTINUE
  5096 CONTINUE
  5094 CONTINUE
    DO 200 J=3,38
    DO 201 K=1,KM
      T(IMP1,J,K)=T(3,J,K)
      TT(IMP1,J,K)=TT(3,J,K)
      T(2,J,K)=T(IM,J,K)
      TT(2,J,K)=TT(IM,J,K)
  201 CONTINUE
  200 CONTINUE
    CALL BARO
    CALL BARO
    AL=COEFFICIENT OF THERMAL EXPANSION
  3 AL=0.2E-3
    ALAL=AL*2.0
    HEAT FLUX ACROSS THE SEA SURFACE IS SPECIFIED AS 70.0*(Q(J)-
    TT(I,J,1)) CAL/DAY
    GAMGAM=H*70.0/(AZ*0.864E5)
    R=6.37E8
    READ(5,1) BB,AAA,BBB

```

```

1 FORMAT(3F10.0)
RR=3.1415926/180.0
RY=AAA*HH
Y=HH*BBB
DO 10 I=1, JMP1
A1=(BB+BBB*FLOAT(I))*HH
X(I)=RY*COS(A1)
10 CONTINUE
CD=14.58E-5/(Y*RY)
DO 9997 J=1,38
XM(J)=(X(J)+X(J+1))/2.0
FJU(J)=CD*(X(J)-X(J+1))
9997 CONTINUE
H2=H*2.0
YY=Y*Y
      AAA AND BBB ARE WEIGHTS IN THE IMPLICIT SCHEME FOR THE INERTIA
C      OSCILLATION
      AAA=0.6
      BBB=0.4
      RR=R*R
      RRH=RR*H
      AL2=AL/2.0
      HH=H*H
      AZHH=AZ/HH
      R2=R*2.0
      AHY=AH*Y
      AQ=245.0*H
      BB=YY*RR
      A1=AM/BB
      AHRR=AH/RR
      BUN=4.0/3.0
      BAN=2.0/3.0
      AMRR=AM/RR
      AH2=AH/BB
      RY=R*Y
      BB=1.0/(Y*R)
      BB2=BB/2.0
      RETURN
      END
      SUBROUTINE BARO
      RETURN
      END
      SUBROUTINE WIND
      RETURN
      END
      SUBROUTINE SHAPE2
COMMON T(147,39,5),TT(147,39,5),SP(147,39),AT(5),UU(147,39,5),
1VV(147,39,5),U(147,39,5),V(147,39,5),W(147,39,5),UB(147,39),
2VB(147,39),WE(147,39),WN(147,39),Q(39),XJA(38),XHT(38),XHS(38),
3 XMY(38),Z(5),XM(39),FU(39),FJU(39),ZZ(6),H,AZ,AH,DT,AL,
4GAM,Y,YY,R,RR,HH,H2,AZHH,R2,AHY,AHRR,AH2,BB,BB2,AAA,BBR,DDT,A1,UV,
5UUU,VVV,RRH,AQ,GAM2,AL2,BUN,RY,AM,AMRR,GAMGAM,ALAL,BAN,KMP1,
6MPP(147,39),MQ(147,39),IM,JM,KM,IMM1,JMM1,KMM1,IMP1,JMP1,MAT,
7 NK,NNNN,IMH,JMH,MATS,L(39),KA(10,39),KB(10,39),LV(39),NEND,
8LA(10,39),LB(10,39),NN
      SUBROUTINE TO BE USED WHEN THE OCEAN SHAPE IS CHANGED.

```

MPP

MPP=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,
=2 ON THE LAND (EXCLUDING THE COAST LINE).
FOR THE COAST-POINTS, REFER TO FIG.1.

14

34XXXXXXXXXXXXXXX33

XXXXXXLANDXXXXXX

XXXXXXXXXXXXXXX

XX?? ?1XX

```

1111          1113
XX             XX
XX23          24XX
XXXXXXXXXXXXXX
31XXXXXXXXXXXX32
12

```

FIG. 1

MQQ

MQQ=1 IF THE FOUR NEAREST SURROUNDING POINTS ARE WATER-POINT,
 =2 ON THE LAND.
 IN OTHER CASES, REFER TO FIG.2.

```

1112
XXXXXXXXXXXXXX
XXXXXLANDXXXX
XXXXXXXXXXXXX
XX1221 2211XX
XX           XX
2111XX      XX1121
XX           XX
XX1122 2112XX
XXXXXXXXXXXXXX
XXXXXXXXXXXXXX
1211

```

FIG. 2

BAROCLINIC PART ONLY. LV(J), LA(I,J), AND LB(I,J) SHOULD BE READ FROM DATA CARDS. THEN, L(J), KA(I,J), KB(I,J), MQQ(I,J) AND MPP(I,J) ARE DETERMINED IN THIS SUBROUTINE.
 THE DATA LV, LA AND LB USED HERE ARE IDENTICAL TO THE DATA LV,
 LA AND LB TO BE USED FOR THE BAROTROPIC PART, BUT IT IS NOT
 THE CASE WITH L, KA AND KB. L, KA AND KB ARE DIFFERENT FROM
 EACH OTHER IN BOTH PARTS.

```

IMM1=IM-1
IMP1=IM+1
JMM1=JM-1
JMP1=JM+1
JMH=3
IMH=3
DO 30 J=1,JM
DO 31 I=1,IMP1
MQQ(I,J)=2
31 CONTINUE
30 CONTINUE
DO 32 J=3,JMM1
READ(5,33) M
33 FORMAT(I2)
READ(5,34) (LA(I,J),LB(I,J),I=1,M)
34 FORMAT(7(2I4,2X))
DO 35 I=1,M
II=LA(I,J)
IG=LB(I,J)
DO 36 N=II,IG
MQQ(N,J)=1
36 CONTINUE
35 CONTINUE
LV(J)=M
MQQ(1,J)=MQQ(IMM1,J)
MQQ(2,J)=MQQ(IM,J)
MQQ(IMP1,J)=MQQ(3,J)
32 CONTINUE
DO 1 J=2,JM

```

```

JMI=J-1
DO 2 I=3, IM
IM1=I-1
IF(MQQ(I,J).EQ.1) GO TO 3
IF(MQQ(IM1,J).EQ.1) GO TO 3
IF(MQQ(IM1,JM1).EQ.1) GO TO 3
IF(MQQ(I,JM1).EQ.1) GO TO 3
MPP(I,J)=2
GO TO 2
3 MPP(I,J)=1
2 CONTINUE
MPP(1,J)=MPP(IMM1,J)
MPP(2,J)=MPP(IM,J)
MPP(IM1,J)=MPP(3,J)
1 CONTINUE
DO 4 J=3, JMM1
MM=LV(J)
WRITE(6,9) J, LV(J), (LA(I,J), LB(I,J), I=1, MM)
9 FORMAT(1H ,20I5)
4 CONTINUE
DO 11 I=3, IM
WRITE(6,12) I, (MPP(I,J), J=3, JM)
WRITE(6,13) (MQQ(I,J), J=3, JM)
12 FORMAT(1H ,I3,2X,38I3)
13 FORMAT(1H ,6X,38I3)
11 CONTINUE
DO 18 J=3, JM
MM=0
MP=MPP(3,J)
IF(MP.EQ.2) GO TO 70
II=3
MM=MM+1
70 DO 50 I=4, IMM1
MPPIJ=MPP(I,J)
IF(MPPIJ.EQ.MP) GO TO 60
GO TO (16 ,200), MPPIJ
16 II=I
MM=MM+1
GO TO 60
200 KA(MM,J)=II
KB(MM,J)=I-1
60 MP=MPPIJ
50 CONTINUE
IF(MPP(IM,J).EQ.2) GO TO 80
KA(MM,J)=II
KB(MM,J)=IM
80 L(J)=MM
WRITE(6,9) J, L(J), (KA(I,J), KB(I,J), I=1, MM)
18 CONTINUE
DO 8004 J=JMH, JM
JP1=J+1
JM1=J-1
DO 8005 I=IMH, IM
IF(MPP(I,J).EQ.2) GO TO 8005
IP1=I+1
IM1=I-1
K=0
IF(MQQ(I,J).EQ.2) K=K+1000
IF(MQQ(IM1,J).EQ.2) K=K+100
IF(MQQ(IM1,JM1).EQ.2) K=K+10
IF(MQQ(I,JM1).EQ.2) K=K+1
IF(K.EQ.0) GO TO 8005
IF(K.EQ.11) GO TO 42
IF(K.EQ.1100) GO TO 1100
IF(K.EQ.110) GO TO 110
IF(K.EQ.1001) GO TO 1001

```

BS

IF(K.EQ.1110) GO TO 1110
IF(K.EQ.1101) GO TO 1101
IF(K.EQ.111) GO TO 111
IF(K.EQ.1011) GO TO 1011
IF(K.EQ.10) GO TO 40
IF(K.EQ.1) GO TO 41
IF(K.EQ.1000) GO TO 1000
IF(K.EQ.100) GO TO 100
100 MPP(I,J)=32
GO TO 8005
1000 MPP(I,J)=31
GO TO 8005
41 MPP(I,J)=34
GO TO 8005
40 MPP(I,J)=33
GO TO 8005
1011 MPP(I,J)=24
GO TO 8005
111 MPP(I,J)=23
GO TO 8005
1101 MPP(I,J)=21
GO TO 8005
1110 MPP(I,J)=22
GO TO 8005
1001 MPP(I,J)=11
GO TO 8005
110 MPP(I,J)=13
GO TO 8005
1100 MPP(I,J)=12
8005 CONTINUE
8004 CONTINUE
DO 7501 J=2, JMM1
JP1=J+1
JM1=J-1
DO 7500 I=2, IM
IF(MQQ(I,J).EQ.2) GO TO 7500
IP1=I+1
IM1=I-1
K=1111
IF(MQQ(IP1,J).EQ.2) K=1000+K
IF(MQQ(I,JP1).EQ.2) K=K+100
IF(MQQ(IM1,J).EQ.2) K=K+10
IF(MQQ(I,JM1).EQ.2) K=K+1
IF(K.EQ.1111) K=1
MQQ(I,J)=K
7500 CONTINUE
MPP(1,J)=MPP(IMM1,J)
MQQ(1,J)=MQQ(IMM1,J)
MPP(IMP1,J)=MPP(3,J)
MQQ(IMP1,J)=MQQ(3,J)
MPP(2,J)=MPP(IM,J)
MQQ(2,J)=MQQ(IM,J)
7501 CONTINUE
MPP(1,JM)=MPP(IMM1,JM)
MPP(2,JM)=MPP(IM,JM)
MPP(IMP1,JM)=MPP(3,JM)
DO 9000 I=1, IMP1
WRITE(6,12) I, (MPP(I,J), J=3, JM)
WRITE(6,13) (MQQ(I,J), J=3, JM)
9000 CONTINUE
RETURN
END

SUBROUTINE GEOST

COMMON T(147,39,5), TT(147,39,5), SP(147,39), AT(5), UU(147,39,5),
 1 VV(147,39,5), U(147,39,5), V(147,39,5), W(147,39,5), UB(147,39),
 2 VB(147,39), WE(147,39), WN(147,39), Q(39), XJA(38), XHT(38), XHS(38),
 3 XM Y(38), Z(5), X(39), XM(39), FU(39), FJU(39), ZZ(6), H, AZ, AH, DT, AL,
 4 GAM, Y, YY, R, RR, HH, H2, AZHH, R2, AHY, AHRR, AH2, BB, BB2, AAA, BBB, DDT, A1, UV,
 5 UUU, VVV, RRH, AQ, GAM2, AL2, BUN, RY, AM, AMRR, GAMGAM, ALAL, BAN, KMP1,
 6 MPP(147,39), MQQ(147,39), IM, JM, KM, IMM1, JMM1, KMM1, IMP1, JMP1, MAT,
 7 NK, NNNN, IMH, JMH, MATS, L(39), KA(10,39), KB(10,39), LV(39), NEND,
 8 LA(10,39), LB(10,39), NN
 HG=H*490.0

JJ=0

DO 20 J=JMH, JM

LJ=L(J)

DO 4011 M1=1, LJ

II=KA(M1, J)

IG=KB(M1, J)

DO 21 I=II, IG

PZ=0.0

PZ1=0.0

DO 4018 K=1, KMM1

KP1=K+1

PZ=PZ-ZZ(KP1)*AL2*(TR(I,J,K)+TT(I,J,KP1))

PZ1=PZ1+PZ*Z(KP1)

4018 CONTINUE

SP(I, J)=PZ1*HG

21 CONTINUE

4011 CONTINUE

20 CONTINUE

DO 4019 J=JMH, JM

SP(IMP1, J)=SP(3, J)

4019 CONTINUE

DO 3000 J=JMH, JMM1

FJUJ=FJU(J)

IF(ABS(FJUJ).LE.1.0E-7) GO TO 3

JP1=J+1

RXMJ=R*XM(J)

R1=RXMJ*FJUJ

RX=RY*FJUJ

GO TO 4

3 JJ=J

GO TO 3000

4 LJ=LV(J)

DO 4002 M1=1, LJ

II=LA(M1, J)

IG=LB(M1, J)

DO 3001 I=II, IG

IP1=I+1

SP0=SP(I, J)-SP(IP1, JP1)

SP1=SP(IP1, J)-SP(I, JP1)

PXBIJ=SP1-SP0

PYBIJ=-SP1-SP0

DO 3002 K=1, KM

ZZK=ZZ(K)

KM1=K-1

IF(K.NE.1) GO TO 4000

PA=0.0

PB=0.0

GO TO 4001

4000 CONTINUE

P1=T(I,JP1,K)+T(I,JP1,KM1)-T(IP1,J,K)-T(IP1,J,KM1)

P2=T(I,J,K)+T(I,J,KM1)-T(IP1,JP1,K)-T(IP1,JP1,KM1)

PA=P1-0.7744*10^-10/P1 P21

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PB-PB+AQ-KAL*(P2-P1)
4001 CONTINUE
  PV=(PA*AQ-PXBIJ)/R1
  PU=(-PB*AQ+PYBIJ)/RX
  U(I,J,K)=PU
  UU(I,J,K)=PU
  V(I,J,K)=PV
  VV(I,J,K)=PV
3002 CONTINUE
3001 CONTINUE
4002 CONTINUE
3000 CONTINUE
  IF(JJ.EQ.0) GO TO 7
  JM1=JJ-1
  JP1=JJ+1
  DO 5 I=IMH,IM
  IF(MQQ(I,JJ).EQ.2) GO TO 5
  DO 6 K=1,KM
  PA=UU(I,JM1,K)
  PB=UU(I,JP1,K)
  PU=VV(I,JM1,K)
  PV=VV(I,JP1,K)
  IF(PA.GT.200.0) PA=0.0
  IF(PB.GT.200.0) PB=0.0
  IF(PU.GT.200.0) PU=0.0
  IF(PV.GT.200.0) PV=0.0
  AU=(PA+PB)/2.0
  AV=(PU+PV)/2.0
  UU(I,JJ,K)=AU
  U(I,JJ,K)=AU
  VV(I,JJ,K)=AV
  V(I,JJ,K)=AV
6 CONTINUE
5 CONTINUE
7 DO 4007 K=1,KM
  DO 4008 J=JMH,JMM1
  U(2,J,K)=U(IM,J,K)
  V(2,J,K)=V(IM,J,K)
  UU(2,J,K)=UU(IM,J,K)
  VV(2,J,K)=VV(IM,J,K)
  U(IMP1,J,K)=U(3,J,K)
  V(IMP1,J,K)=V(3,J,K)
  UU(IMP1,J,K)=UU(3,J,K)
  VV(IMP1,J,K)=VV(3,J,K)
4008 CONTINUE
4007 CONTINUE
  CALL CONTI
  DO 7002 K=2,KM
  WRITE(6,7001) K
7001 FORMAT(1H,23HORIZONTAL VELOCITY AT K=I1)
  DO 7003 I=IMH,IM
  WRITE(6,7000) I,(W(I,J,K),J=3,20)
7000 FORMAT(1H,I3,1X,18F7.2)
7003 CONTINUE
  DO 7024 I=IMH,IM
  WRITE(6,7000) I,(W(I,J,K),J=21,38)
7024 CONTINUE
702 CONTINUE
  DO 7009 K=1,KM
  WRITE(6,7010) K
7010 FORMAT(1H,7HU AT K=I1)
  DO 7011 I=IMH,IM
  WRITE(6,7012) I,(UU(I,J,K),J=3,20)
7012 FORMAT(1H,I3,2X,18F5.0)
7011 CONTINUE
  DO 7022 I=IMH,IM

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    WRITE(6,7012) I,(UU(I,J,K),J=21,38)
7022 CONTINUE
      DO 7021 I=IMH,IM
        WRITE(6,7012) I,(VV(I,J,K),J=3,20)
7021 CONTINUE
      DO 7023 I=IMH,IM
        WRITE(6,7012) I,(VV(I,J,K),J=21,38)
7023 CONTINUE
7009 CONTINUE
      RETURN
      END
```